

Prepared for MAUNSELL/AECOM

Darling River Water Savings Project
Hydrology Evaluation
of
Key Options

FINAL REPORT - MAY, 2007

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EXECUTIVE SUMMARY

This report evaluates the potential water saving volumes and associated impacts for a range of core options in the Darling Basin, focussing primarily on those at Menindee Lakes. The Menindee Lakes Scheme has a full supply capacity of 2,050 Gigalitres and provides water for New South Wales, South Australian, and Victorian purposes. The shallow expansive nature of the lakes scheme results in considerable losses through evaporation. The full extent of this is manifested in streamflows, which are 23% less below the lakes than the flows immediately upstream.

The results from this report will be used as input into the development of water saving strategies for the basin as part of the Darling River Water Savings Project. As such the options in this report should not be viewed as water saving strategies, but rather as components to strategies.

The magnitude of all water savings in this report has been determined at the source. However, the consequences of savings in terms of changes to river flows and consumptive reliability have been assessed wherever possible over a wider area including both the Lower Darling and Murray Rivers.

Water savings have been quantified using a mix of observed data, together with results from sophisticated computer models. Hydrologic modelling for this project has been carried out using the Murray Monthly Simulation Model (MSM), (Close, A.F. 1986). This model is the principle water planning tool for the Murray and Lower Darling River systems.

Options that were assessed using modelling are:

- Base Case - The base case (current operation and development)
- M0 - Rapid emptying of the Scheme in the range of 480GL to 200GL
- M1 - Rapid emptying of the Scheme in the range of 480GL to 300GL
- M2 - Rapid emptying of the Scheme in the range of 680GL to 100GL
- M3 - Rapid emptying of the Scheme in the range of 300GL to 100GL
- NoMC - More natural wetting and drying of Lake Menindee and Lake Cawndilla
- NoCExMO - More natural wetting and drying of Lake Cawndilla
- NoCEnMO - More natural wetting and drying of Lake Cawndilla
- NoMExCO - More natural wetting and drying of Lake Menindee
- NoMEnCO - More natural wetting and drying of Lake Menindee
- MCell - Construction of two Menindee Lake cells
- 0.5M - Construction of a two Menindee Lake cells (One Filled)
- Plnc - Increasing the capacity of Lake Pamamaroo
- Potential water savings from privately owned storages.

Options that were assessed using observed data on flows, losses and infrastructure performance are:

- Improved extraction from residual pools in the Menindee Scheme.
- Improved use of existing smaller deeper lakes in the Menindee Scheme.
- Utilisation of existing and new storages upstream of the Menindee Scheme.

- Utilisation of existing and new storages downstream of the Menindee Scheme.

Menindee Scheme Saving Options

Evaporative savings and diversion changes from modelled scheme options are presented in Tables E1 and E2.

All but one of the modelled options produces evaporative water savings. The exception is the option for increasing the capacity of Lake Pamamaroo. For this option the savings created by increased storage in Lake Pamamaroo is exceeded by the additional evaporative losses incurred in Lake Wetherell.

All but two options produce reductions in Lower Darling diversions of greater than 5%. For all options, diversion changes for New South Wales, Victorian and South Australian Murray users is small.

Out of all restoration options, restoration of both Menindee and Cawndilla Lakes to more natural wetting and drying cycles achieves the biggest evaporative saving of 211 Gigalitres per annum. However, this option also has the largest reduction in irrigation diversions (75% in the Lower Darling).

Out of all rapid emptying options, emptying in the range of 680GL to 100GL gives the biggest evaporative saving of 91 Gigalitres per annum. Lower Darling diversions are reduced by 13%. Murray diversions are largely unchanged.

Table E1 – Key Modelled Options - Evaporative Savings (GL/Yr)

Option	Wetherell Net Evap	Pamamaroo Net Evap	Menindee Net Evap	Cawndilla Net Evap	Total Net Evap (GL/Yr)	Decrease From Base Case (GL/Yr)
Base case	50	82	168	126	426	0
M0	62	77	128	105	372	-54
M1	64	81	133	108	387	-39
M2	55	69	117	95	335	-91
M3	69	81	143	113	406	-20
NoMC	117	94	5	0	215	-211
NoCExMO	80	91	183	0	353	-73
NoCEnMO	82	92	176	0	351	-76
0.5M	56	84	87	130	357	-70
NoMExCO	75	83	0	134	291	-136
NoMEnCO	83	92	0	118	292	-134
PInc	65	86	162	123	435	+9
MCell	50	82	130	123	388	-38

Table E2 – Longterm Average Diversion Change (GL/Yr)

Year	Total NSW Lower Darling Div (GL/Yr)	Decrease from Base Case (GL/Yr)	Total NSW Div (GL/Yr)	Decrease from Base Case (GL/Yr)	Total Vic Div (GL/Yr)	Decrease from Base Case (GL/Yr)	Total SA Div (GL/Yr)	Decrease from Base Case (GL/Yr)
Base case	129		1966	0	1675		1139	
M0	119	-10	1979	13	1671	-4	1143	4
M1	121	-8	1986	20	1674	-1	1143	4
M2	112	-17	1969	3	1665	-10	1145	6
M3	124	-5	1979	13	1673	-2	1144	5
NoMC	32	-97	1922	-44	1636	-39	1141	2
NoCExMO	55	-74	1968	3	1670	-5	1142	3
NoCEnMO	55	-74	1969	3	1671	-4	1142	3
0.5M	116	-13	1968	2	1675	0	1142	3
NoMExCO	116	-13	1963	-2	1673	-2	1142	3
NoMEnCO	112	-17	1964	-2	1672	-3	1143	4
PInc	122	-7	1966	0	1675	0	1140	1
MCell	129	0	1966	0	1675	0	1139	0

Flow changes resulting from key modelled options are presented in Tables 11 and 12 within the report. With the exception of the option for increasing the capacity of Lake Pamamaroo, all options produce increased flows in the Lower Darling. Most options also reduce the volume of flow released and spilt from Lake Cawndilla.

Flows in the Murray upstream of Wentworth are largely unchanged by water saving options at the Menindee Scheme. The largest change of 80 Gigalitres per annum occurs with restoring Lakes Menindee and Cawndilla to natural wetting and drying cycles.

Flows downstream of Wentworth generally increase in most options. This results in increased spills from Lake Victoria and a corresponding reduction in Lake Victoria regulated releases. Flows across the South Australian border also increase for most options.

Modelled options produce changes in salinity concentrations both within and downstream of the lakes scheme. Restoration of Lakes Menindee and Cawndilla to more natural wetting and drying cycles result in an increase in average salinity in the other lakes. However, restoration of Lake Menindee alone results in a reduction in average salinity in Lakes Cawndilla and Wetherell. The average salinity in Lake Pamamaroo is also improved if the Cawndilla outlet capacity is increased.

Restoration of Lake Cawndilla to a more natural wetting and drying cycle results in a reduction in salinity in Lake Pamamaroo, an increase in salinity in Lake Menindee and negligible change in Lake Wetherell. Options that involve rapid emptying of the lakes appear to result in increased lake salinity levels.

Downstream of the scheme, average salinity levels generally increase in the Lower Darling and the Murray for options that involve restoration of the lakes to more natural and wetting and drying cycles. However, for options that involve more rapid

emptying of the lakes, average salinity levels decrease both in the Lower Darling and in the Murray.

Off River Storage Saving Options

Three potential water savings options with respect to reducing evaporation from off river storages were evaluated for a Namoi Valley case study. These consisted of

1. Purchasing of all supplementary licenses.
2. Decommissioning off river storages and enlarging Keepit and Split Rock Dams.
3. Reducing evaporation by covering off river storage surface area.

Reduced access to supplementary water was found to be offset by increased general security and floodplain harvesting usage. As a result, reduction in evaporation from off-river storages was negligible. Reduced access to supplementary water does however increase the Namoi end of system flows by 13 Gigalitres per annum.

Removal of off river storage capacity and a corresponding increase in the capacity of Keepit and Split Rock Dams results in increased evaporative losses from Keepit and Split Rock. However, this is more than offset by the reduction in evaporation from off-river storages. The total saving in evaporation from this option is 55 Gigalitres per annum. The major impact from this saving strategy is the large decrease in valley diversions. Therefore enlargement of Keepit and Split Rock cannot offset the impacts of removal of off-river storage.

Covering off river storages results in extra water in the storages and evaporative savings of 79 Gigalitres per annum. This extra water allows users to divert less water and plant a greater area. An additional benefit is that the average volume in Keepit and Split Rock Dam also increases with little change in major storage evaporation.

More Efficient Instream and Floodplain Storage Saving Options

Creation of Instream and floodplain storage upstream and downstream of the Menindee Scheme has been assessed as potentially being more efficient than storing water in the Menindee Scheme.

Instream and floodplain storage immediately upstream of the Menindee Scheme will result in reduced evaporative volumes when compared to the equivalent volume being stored at the Menindee Lakes Scheme. However, additional instream and floodplain storage has to approach in excess of 140 Gigalitres for a surface area of 5,200Ha before any appreciable evaporative savings can be made.

The small volume of instream storage in the Lower Darling below the Menindee Scheme means that its usefulness in terms of storage and reduction in evaporative losses is severely limited. Consequently, no further assessment of this option has taken place.

The viability of storage of water in existing tributary major dams has also been assessed. Possible locations for storage and supply of Lower Darling volumes are:

- Keepit Dam on the Namoi River,
- Chaffey Dam on the Peel River,
- Pindari Dam on the Macintyre River.

A preliminary assessment of delivery losses associated with differing storage and delivery volumes from Keepit Dam to the Lower Darling in critical supply years was undertaken using historic information. Losses of 50% in the Namoi and an initial loss of 30 Gigalitres (for Weir filling) and a continuing loss of 15% were assumed in the Barwon Darling.

Losses associated with delivery of water from Keepit Dam and evaporation from the Menindee Scheme are similar in magnitude. However, there may be an environmental and riparian benefit to the losses associated with delivering water from upstream. Evaporative losses have no such benefit.

In conclusion, hydrologic analysis of key options has indicated that that significant water savings have been found to be possible both at the Menindee Scheme and elsewhere in the Darling Basin. However the consequences of this with respect to alterations in diversion volumes, increased salt concentrations and flow changes appears to be high.

1 INTRODUCTION

1.1 Purpose and Content of the Report

The opportunity for water savings in the Darling Basin lies primarily through reduction of evaporative losses from the many storages that are used to enhance supply reliability for the annual cropping regimes that predominate. The long-term net evaporative losses for the various types of storages that exist within the Darling Basin are presented in Table 1.

Table 1- Net Evaporative Losses for Water Impoundments ¹

<i>Valley</i>	<i>Major Dams</i>	<i>Hillside Dams ^a.</i>	<i>Ring Tanks</i>	<i>Total</i>
Border Rivers	29	55 ^a	125	209
Moonie	0	78 ^a	0	78
Gwydir	31	49 ^a	109	189
Namoi/Peel	52	187 ^a	52	291
Macquarie	56	128 ^a	56	240
Condamine	57	214 ^a	194	465
Balonne				
Nebine	0	0	0	0
Warrego	0	16 ^a	0	16
Paroo	0	0	0	0
Barwon Darling	0	0	94	94
<i>Total Upper Darling Basin</i>	225	727 ^a	630	1582
Lower Darling	393	0	20	413
<i>Total Darling Basin</i>	618	727 ^a	650	1995

Note

^a There is some doubt concerning hillside dam sizes. This also means there is doubt about the accuracy of these evaporation estimates. Whether these figures are net or gross evaporation has not been clarified.

^b This figure includes all the small weirs. Annual Losses from Beardmore Dam, Leslie Dam, Jack Taylor Weir, Moolabah Weir and Buckinbah Weir combined are approximately 40 GL.

In almost all cases the majority of these storages reside on farm and in private ownership. The exceptions to this are the government owned storages. These are typically constructed in the incised valleys that characterise the headwaters of the Darling tributaries. The low evaporative and high rainfall regimes in these regions, together with large storage depths and small surface areas give rise to small net evaporative losses. As a consequence, the opportunity for savings from these storages is small. This can be seen in Table 1, where the major dams in the Upper Darling basin only account for a combined evaporative loss of 225 Gigalitres per annum, compared to 727 Gigalitres per annum for hillside dams and 630 Gigalitres per annum for ring tanks.

¹ Source; MDBC - State of the Darling Interim Hydrology Overview Report- 2006

One exception to this major dam trend is the government owned Menindee Lakes Scheme. The scheme has a full supply capacity of 2,050 Gigalitres and provides water for both New South Wales, South Australian, and Victorian purposes. Utilising existing natural lakes for storage, the shallow expansive nature of the lakes scheme results in considerable losses through evaporation. The full extent of this is manifested in streamflows, which are 23% less below the lakes than the flows immediately upstream. A further example of the scale of evaporative losses can be seen in Figure 1, which shows the resource distribution required to meet Broken Hill and High Security and Riparian requirements for New South Wales when dry times exist. As can be seen the evaporative loss component of the available resource is considerable.

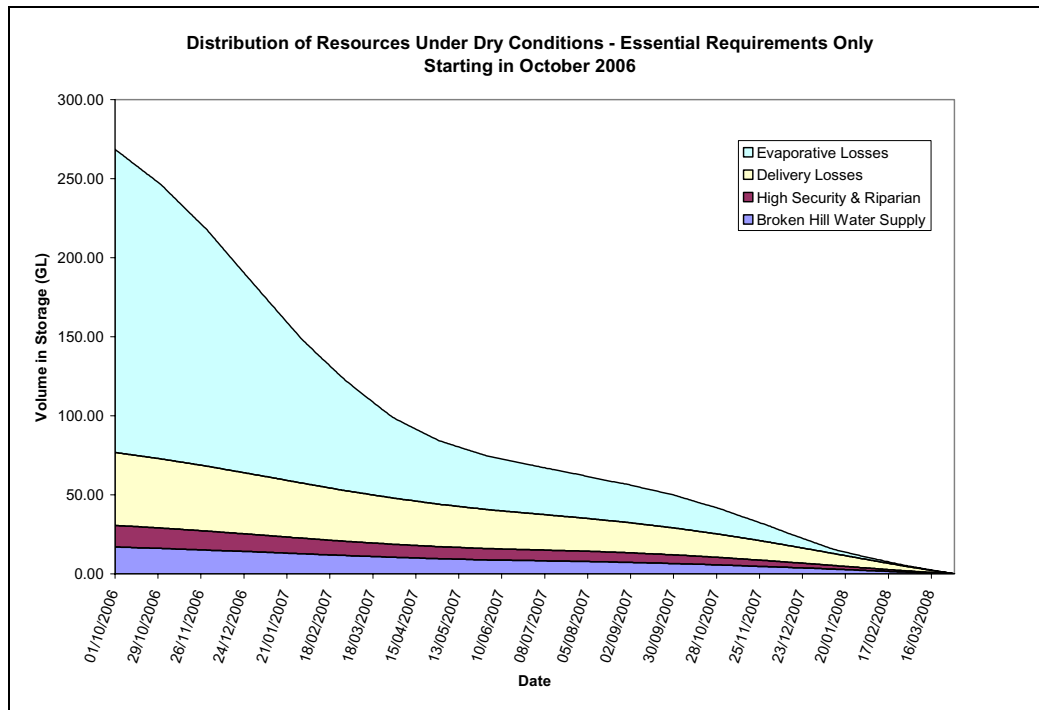


Figure 1 – Distribution of Resources under Dry Conditions

Demands on the Menindee Scheme include providing water for Broken Hill and for adjacent and downstream water users in the Lower Darling. The scheme is also used by both New South Wales and Victoria to provide entitlement and dilution flows to South Australia in accordance with the Murray Darling Basin Agreement. Some flood mitigation benefit from the scheme is also possible. However, this is heavily dependent upon storage volumes and operational practices.

Historically, lake management has aimed to maximise the potential supply reliability, ensure ecological sustainability and to maximise water quality of water within the lakes and the Lower Darling River. Operational objectives can be summarised as:

- minimise lake evaporation,
- maximise lake storage volumes,

- maximise water quality in terms of salinity, and blue green algae (cyanobacterial) blooms,
- maximising ecological benefits, including fish and wildlife habitat,
- control of foreshore erosion.

This report provides a hydrologic assessment of the potential significant water saving volumes that can be made from structural and operational strategies at both Menindee Lakes and the greater Darling Basin. Information from this report will be used as input into the option and strategy evaluation process for realising significant water savings in the Darling River.

The significance of a water saving volume is dependant upon both its size and when it occurs. A small saving volume in a time of resource shortage is likely to be just as important as a large volume when resources are plentiful. This has been borne in mind when selecting key saving options and throughout the hydrologic assessment process.

In conducting the hydrologic analysis the magnitude of water savings has been determined at the source. However, the consequences of savings in terms of changes to river flows and consumptive reliability have been assessed wherever possible over a wider area.

Due to the short study timeframes the methodology for assessing water savings for each option has varied. Wherever possible, a quantitative analysis using existing hydrologic models and data has been undertaken. However, in some instances a qualitative assessment of the likely magnitude of water savings and consequences has had to be made.

2 MENINDEE LAKES OPERATION

2.1 Target Storage Operation

Operation of the lakes scheme mainly consists of movement of water between the interconnected lakes, and supply of water to meet downstream demands whilst minimising evaporative losses. Evaporation in the area is approximately 2.5 metres (426 Gigalitres per annum) a year.

Based on discussions with staff from the Department of Natural Resources and State Water, the preferred lake filling strategy is to:

1. Fill Lake Wetherell to 59.8 metres AHD.
2. Fill Lake Pamamaroo to full supply level (60.45 metres) (filling Lakes Pamamaroo and Wetherell simultaneously above 59.8 m).
3. Fill Lake Menindee/Cawndilla to full supply level (59.84 metres).
4. Fill Lake Wetherell to full supply level (61.67 metres).
5. Surcharge Lake Pamamaroo (61.5 metres) and Lake Wetherell (62.3 metres), and then Lakes Menindee and Cawndilla (60.45 metres).

In most instances the procedures for releasing water from the lakes are generally the reverse of this, with all immediate consumptive demands being firstly met from Lake Menindee and Lake Cawndilla and Lake Wetherell above 59.8 m.

2.2 Releases to the Great Darling Anabranh and Lake Tandou

Lake Cawndilla discharges into the Darling Anabranh via Tandou Creek with the water level being maintained by a regulator at Packers Crossing. The lake is primarily used to supply demands along this system. The main user of water from the lake is Tandou Pty Ltd. Tandou Pty Ltd syphons water to its irrigation development at Lake Tandou. Generally, rates of release from Lake Cawndilla range from 200 to 500 Megalitres a day depending upon seasonal conditions. The Cawndilla outlet regulator has a capacity of 2,000 Megalitres per day but seldom operates at this due to head limitations.

The Pennelco pumps on the Lower Darling River are used to supply Tandou Pty Ltd when insufficient resources are available from Lake Cawndilla. These pumps are not operated to supply other water users or the Anabranh.

A pipeline to supply stock and domestic uses and environmental watering along the anabranh is currently being constructed. When finalised, this pipeline will see a change to the operation of the Menindee Lakes system.

2.3 Interstate Commitments

When the combined volumes of the Lakes exceed 480 Gigalitres during a draw down phase and 640 Gigalitres during a filling phase, water may be released to the Lower Darling River as requested by the Murray-Darling Basin Commission (MDBC). When MDBC resources are available in Menindee Lakes, releases from the Hume Reservoir are made only to the extent to meet minimum flow requirements at Euston on the River Murray.

The MDBC will generally specify releases from Menindee Lakes when:

- total storage in the lakes is greater than 480 Gigalitres, and
- there is insufficient flow in the River Murray and storage in Lake Victoria to meet South Australia's flow requirement to maintain storage in Lake Victoria at or above specified target volumes.

Throughout these periods of MDBC control, operation of the Lakes is still optimised in order to minimise evaporative losses and maximise water available to supplement River Murray flows by transferring water from the Menindee Lakes to Lake Victoria.

Demands on the Lake system when in MDBC control can be up to 7,000 Megalitres per day, although higher releases may be required under certain circumstances such as a very dry season with high Murray River irrigation demand, or if storage in Lake Victoria is below target prior to the start of the irrigation season. The maximum regulated flow rate in the Lower Darling is between 9,000 and 9,500 Megalitres per day. Release rates of 7,000 Megalitres or more exceed the outlet capacity of any of the individual regulators, other than the main weir, leading to demand being usually supplied from two or more lakes.

2.4 Drought Management

The Menindee Lakes Scheme was constructed to provide for water conservation. Consequently, management for drought conditions forms an important aspect of operation of the lakes.

When the total storage volume within the scheme falls to 480 Gigalitres, all rights to the water remaining in storage reverts to New South Wales, and supply is primarily for Lower Darling water users only.

The 480 Gigalitres can potentially provide security of supply to all adjacent and downstream users for one year under a zero inflow scenario. This assumes that all entitlements are fully utilised. In most cases, entitlements are not fully utilised and this under usage extends supply potential beyond one year.

More often than not when the scheme falls to 480 Gigalitres, the upstream catchments can be in extended drought. This is not uncommon in the Darling with the scheme dropping below 480 Gigalitres in 50% of **years** and as shown in Figure 2 for 20% of the time.

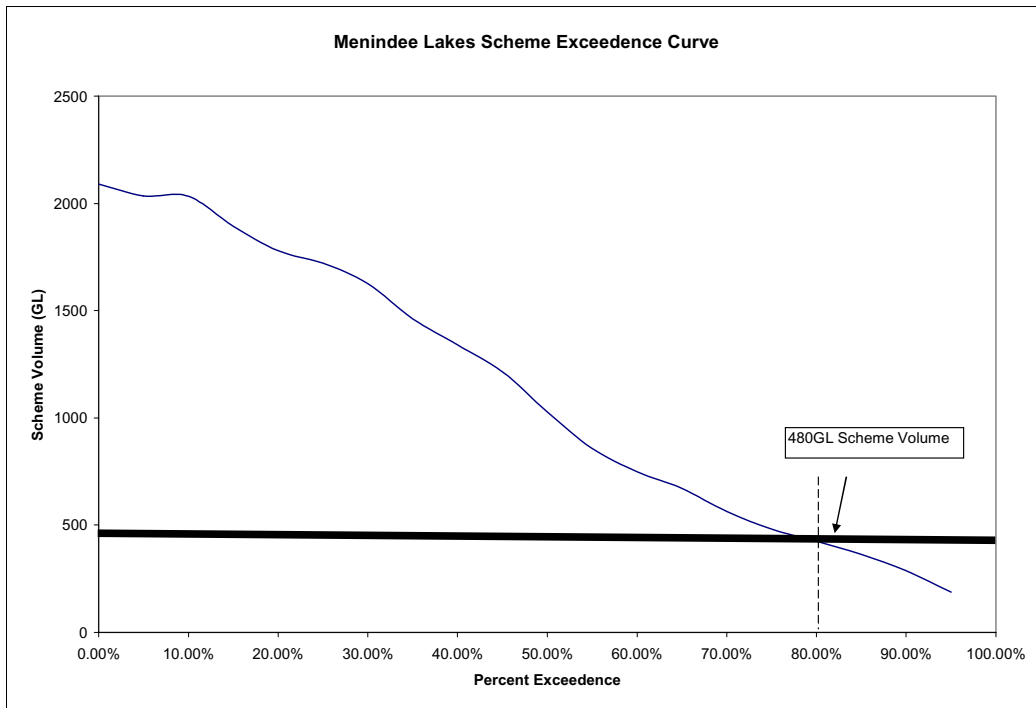


Figure 2 – Menindee Scheme Volume Exceedence Curve

Although the scheme can supply all users for one year when at 480 Gigalitres, a continuing drought results in the availability of water for licensed consumptive use on the Lower Darling being reduced, and restrictions being imposed. The priority for maintaining supply for different purposes is prescribed in the Water Management Act 2000. Under the Act, priority for security of supply aims to ensure adequate supplies in the following order:

- town water supply and riparian entitlement for domestic supply,
- riparian entitlement for stock supply,
- high security for permanent plantings (horticulture and vines),
- general security for non-permanent plantings (pasture and cereal crops).

A typical lake volume distribution with respect to demands when the lakes are within New South Wales control and under prolonged drought is shown in Figure 3. At the commencement of drought management (typically at volumes of 275 GL), resources in the scheme are sufficient to supply Broken Hill and High Security and Riparian users for 18 months.

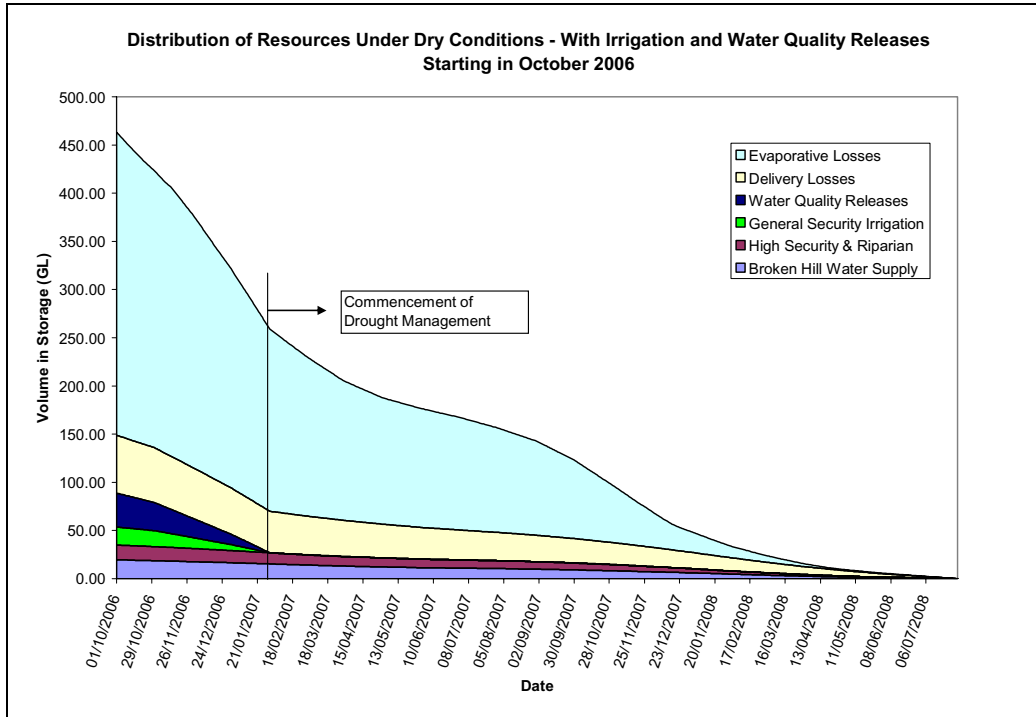


Figure 3 – Distribution of Scheme Resources When In NSW Control

2.5 Flood Management

The severity of floods in the Menindee Lakes and the Lower Darling River is dependent on:

- the volume, peak and duration of floods upstream,
- the volume currently stored in the Lakes,
- the level of lake surcharge adopted during a flood event.

The primary objective of flood operations is to ensure the safety of the structures and to minimise damage to downstream property. The lakes scheme was primarily not built to provide flood mitigation. In most instances the benefit of the lakes for the purposes of flood mitigation is small, due to the limited lake storage capacity relative to the cumulative volume of floodwaters.

Floods in the Darling River (which commences at the confluence of the Culgoa and Barwon rivers) are dependent upon rainfall events generating floods in the catchments of the major upstream tributaries. The relative distribution of flows to the Darling River from Queensland and New South Wales tributaries is shown in Figure 4. The travel time of floodwaters from these upper catchments to the lakes can be up to three months and accurately predicting the volume, duration and peak of a flood is difficult, particularly when Darling River tributaries closer to Menindee, including the Paroo and Warrego Rivers, contribute inflow. The long flood travel times in the Darling River mean that some additional capacity can be realised by pre-releasing stored volumes before the flood arrives at the scheme.

3 DARLING RIVER WATER SAVINGS OPTIONS

3.1 Tools for Determination of Water Savings

Water savings have been quantified using a mix of observed data, together with results from sophisticated computer models.

Numerous options for potential significant water savings within the lakes have been identified in this study. Some options lend themselves to computer modelling whilst others require an assessment using observed information for river flow, losses and infrastructure volumes.

The computer models allow the long-term hydrologic effects of development, water use and structural and operational changes in river management to be assessed in a consistent and detailed way. Computer models of river systems are, necessarily, simplified representations of the many complicated interactions between the many factors that affect river flows. The complex and variable nature of the basin's hydrology, and the changing scale and effect of water use development, mean modelling is the most reliable way to assess the impact current development and management arrangements on long-term water savings and flow outcomes.

Hydrologic modelling for this project has been carried out using the Murray Monthly Simulation Model (MSM), (Close, A.F. 1986). This model is the principle water planning tool for the Murray and Lower Darling River systems.

3.2 Description of Modelled Water Saving Options

3.2.1 General

For those options that can be modelled, detailed modelling of every option in the short study timeframe is not possible. This is further complicated by the true extent of water savings usually only being realised through the integration of individual "saving options".

Fortunately, as all options seek to produce significant savings through combinations of reduction in demand, reduction in lake storage time, and reduction in lake storage area, it is possible to assess key options that can then be used to infer savings for the larger option suite. Key options for which water savings were assessed using the detailed model are:

Key Modelled Options

- The Base Case (Current Operation and Development).
- Increasing the release rate from the Lakes when in NSW control.
- Variation to dilution flow release patterns.
- Restoration of more natural wetting and drying cycles for Lake Menindee and Lake Cawndilla.
- Restoration of more natural wetting and drying cycles for Lake Menindee.
- Restoration of more natural wetting and drying cycles for Lake Cawndilla.
- Construction of a two cells in Lake Menindee (Both Filled).
- Construction of two cells in Lake Menindee (One Filled).
- Increasing the Capacity of Lake Pamamaroo.
- Potential water savings from privately owned storages.

Restoration options entail utilising the lakes for flood mitigation purposes only.

3.2.2 The Base Case (Current Operation and Recent Development)

The base case is used as a benchmark comparison with respect to all water savings options. The base case ideally represents current management, and operational practices as well as current infrastructure volumes and resource demands.

This base case is the same as that used for the Menindee EIS Project, and includes the anabranch pipeline with an environmental release of 60GL every two years on average. It also assumes use of the Penelco pumps to supply Tandou Pty Ltd when resources are unavailable from Lake Cawndilla.

The current scheme inflow data in the base case reflects varying levels of development upstream of the Lakes. Around the mid 1990's the MDBC updated their estimate of the Menindee Scheme monthly inflows by adjusting the pre-development flow dataset for upstream New South Wales development at that time based on New South Wales model results. Therefore, the model inflow data reflects mainly mid 1990's New South Wales development levels. The inflow set does not incorporate the reduced flows caused by growth in Queensland in the Late 1990's. Whilst reduced inflows will reduce Lake Evaporation, changes in Lake Evaporation from the benchmark are likely to be unaffected.

The filling strategy adopted in the model base case is:

1. Fill Lake Wetherell to 59.8 metres AHD.
2. Fill Lake Pamamaroo to full supply level (60.45 metres).
3. Fill Lake Menindee/Cawndilla to full supply level (59.84 metres).
4. Fill Lake Wetherell to full supply level (61.67 metres).
5. Surcharge Lake Pamamaroo (61.5 metres) and Lake Wetherell (62.3 metres), and then Lakes Menindee and Cawndilla (60.45 metres).

The maximum storage volumes adopted in the model are presented in Table 2.

Table 2 – Modelled and Current Lake Maximum Volumes

Lake	Base Case Maximum Volume (GL)	Current Operational Maximum Volume (GL)
Wetherell	262	262
Pamamaroo Copi Hollow	350	350
Menindee	719	631
Cawndilla	705	631
Total Scheme Volume	2049	1874

The assumed residual storages in the base case for each of the lakes are presented in Table 3². As can be seen, the modelled base case residual storage volumes differ

² At the time of preparing this report the with the exception of Lake Cawndilla, the accuracy of the Menindee Scheme capacity table at low levels is thought to be good, with bathometric surveys of Wetherell and Pamamaroo, and aerial mapping of Lake Menindee having taken place. A more accurate survey of the lower parts of Lake Cawndilla may be warranted given the importance of the residual pool volume.

somewhat from the advised Department of Natural Resources (DNR) residual storage volumes. The greatest difference is in the assumed residual pool volume for Lake Cawndilla.

Table 3 – Modelled Residual Storage

Lake	Base Case Residual Volume (ML)	Advised Residual Volume (ML)
Lake Cawndilla	9,620	100,970
Lake Menindee	88,000	71,190
Lake Pamamaroo	10,063	31,730
Lake Wetherell	390	12,376
Total Residual Storage	108,640	216,266

Differences between base case and actual residual pool volumes will affect the volumes of savings identified in this report. In the case of Lake Cawndilla, the modelled base case assumes that stored volumes in the range of 100 Gigalitres to 9.6 Gigalitres can be released through the existing outlet works. In practice, lowering of the storage from 100 Gigalitres to 9.6 Gigalitres will require pumping. It is likely that if the base case were adjusted to reflect an appropriate residual pool volume of 100 Gigalitres then savings identified in this report will be increased for any option that incorporates works capable of accessing the residual pools. The magnitude of increase will be commensurate with the frequency at which these residual pool volumes are accessed over the period of model simulation and the amount of difference between the base case and advised residual pool volume.

It should also be noted that the Lake Wetherell capacity table in the modelled base case does not include an adjustment for dead storage in Lakes Tandure, Balaka, Malta, or Bijjijie. The Lake Menindee capacity table does not include Lake Speculation. The Lake Cawndilla capacity table includes Lakes Spectacle, Morton Boolka, Cawndilla Ck, and Lake Eurobilli, and the Lake Pamamaroo capacity table includes Copi Hollow with an adjustment for Copi Hollow dead storage of 2,800 Megalitres.

When the volume of water in Lakes Menindee and Lake Cawndilla reaches (55.46), Lake Cawndilla becomes isolated from Lake Menindee. Water can then only be released from Lake Cawndilla through the Cawndilla outlet regulator. At the time of isolation, the stored volume for the base case in Lake Cawndilla is 164 Gigalitres. State Water has advised that a more appropriate estimate is 212 Gigalitres. The effect of this on modelled options is that the evaporative savings as a result of improved works at Lake Cawndilla are likely to be slightly underestimated.

The modelled base case does not incorporate the current drought security arrangements of Figure 1. Consequently, the impact of some options on general security users may be slightly overstated. Despite not incorporating current drought security measures, the lakes scheme does not run out of water under the benchmark scenario. As a consequence, from a quantity perspective sufficient resources are available to meet Broken Hill and High Security requirements over the simulation period.

3.2.3 Increasing the Release Rate from the Lakes when in NSW Control

When the lakes are in New South Wales control and being drawn down for New South Wales requirements, a volume of water sufficient to allow Broken Hill town water supply, high security and riparian demands to be met over an 18 month window assuming no lake inflows is set aside. A significant portion of this volume is for evaporative losses, with volumes increasing if the 18 month window includes two summer periods. This was shown previously in Figure 1.

A number of scenarios whereby the release rates from the lakes is increased when in New South Wales control (below 480 and 680 Gigalitres) have been modelled. Without any clear guidelines on how this water might be released or used, the model was setup to just achieve a monthly target volume of 200 Gigalitres per month at Burtundy (bottom of Lower Darling River) that would simulate the extra water being transferred through to South Australia. The following options were simulated with the model.

- Rapid emptying of the Scheme in the range of 300GL to 100GL.
- Rapid emptying of the Scheme in the range of 480GL to 200GL.
- Rapid emptying of the Scheme in the range of 480GL to 300GL.
- Rapid emptying of the Scheme in the range of 680GL to 100GL.

3.2.4 Variation in Dilution Flow Release Patterns

Under the Murray Darling Basin Agreement, additional releases of 58 Gigalitres per month are made from the Menindee Lakes Scheme to provide dilution flows for South Australia. Variation of this pattern to allow delivery of dilution flows over a shorter time period may have the potential to produce water savings whilst still reducing salinity at Morgan. The viability of this water saving option will be heavily dependent upon channel capacity constraints and the changed dilution pattern resulting in substantial reduction in average surface area.

3.2.5 Restoration of Lakes to more Natural Wetting and Drying Cycles

Reducing the frequency of lake filling will produce water savings, with greater reductions in filling leading to greater savings. The lake exceedence volumes for the scheme and individual lakes are shown in Figure 5. A number of options that aim to restore one or more lakes to natural drying cycles were evaluated. These are discussed in the following sections.

More Natural Wetting and Drying of Lake Menindee and Lake Cawndilla

In this option both Lake Menindee and Lake Cawndilla are restored to a more natural cycle of wetting and drying. In modelling this option, the volumes into Lake Menindee and Lake Cawndilla was reduced to zero by constraining the Lake Menindee inlet regulator capacity. In reality, implementation of this scenario would see the lakes still being utilised during flood times. Unfortunately, this flood mitigation behaviour cannot be represented in the model. As a consequence, any calculated water saving amounts will have to be reduced to account for the short durations of times that the lakes are used for flood mitigation purposes.

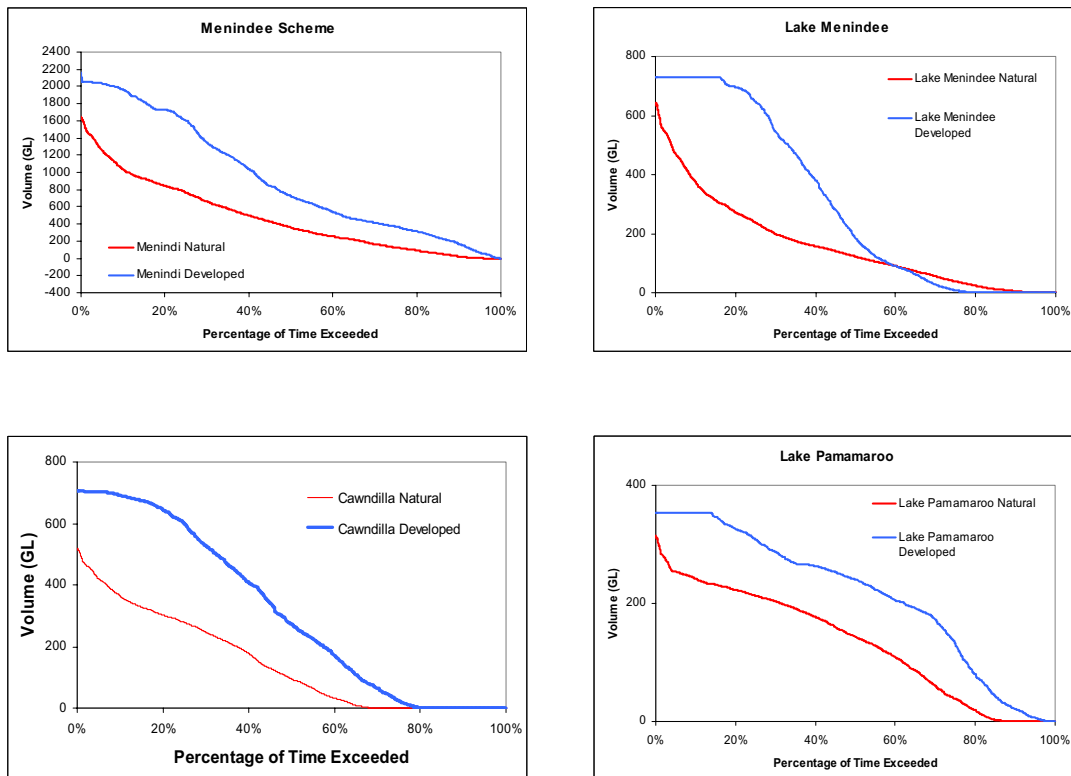


Figure 5 – Natural and Benchmark Lake Exceedence Volumes

More Natural Wetting and Drying of Lake Menindee

An alternate option involves restoration of only Lake Menindee to a more natural regime of wetting and drying. Implementation of this scenario, assumes that water will enter Lake Cawndilla from Lake Pamamaroo via an alternate means. This could be either by construction of a supply channel through or around the outer edge of Lake Menindee. In modelling this option it was assumed that the storage volume versus area relationship for Lake Cawndilla is identical to that which currently exists. This assumption is reliant on the construction of a block bank between the two lakes.

Two variations of this saving option were modelled:

- i) The first with the existing outlet regulator for Lake Cawndilla.
- ii) The second with an increased Cawndilla regulator outlet capacity of 6,000 Megalitres per day to the Lower Darling river.

The second run tries to compensate for the reduction in available outlet capacity as a result of the more natural wetting and drying of Lake Menindee.

More Natural Wetting and Drying of Lake Cawndilla

This option is similar to the proceeding Lake Menindee option in that Lake Cawndilla is restored to a more natural cycle of wetting and drying. Implementation of this option will involve the construction of a block bank and regulator across Morton

Boolka in order to fill Lake Menindee to its current capacity and allow volumes into Lake Cawndilla during times of floods.

Two variations of this saving option were modelled:

- i) The first with the existing outlet regulator for Lake Menindee.
- ii) The second with an increased Menindee regulator outlet capacity of 10,000 Megalitres per day.

The second run tries to compensate for the reduction in available outlet capacity as a result of the more natural wetting and drying of Lake Cawndilla.

3.2.6 Construction of a Two Menindee Lake Cells (Both Filled)

Splitting of Lake Menindee into two cells with appropriate regulators or pumps to allow efficient filling and emptying of each cell potentially allows for increased operational flexibility. For the purposes of modelling, it has been assumed that each cell can hold fifty percent of the existing lake storage volume for fifty percent of the existing lake storage area. This means that the storage volume area relationship for each cell is effectively half that of the total lake relationship. Target storage operation of the scheme and draw down of Lake Cawndilla via the existing Menindee outlet regulator remains unchanged when the lakes are connected.

Modelling has also assumed that draw down of each Menindee Lake cell is able to be achieved using the existing Menindee outlet regulator. However, construction of the two cells will result in the outlet being able to deliver the same discharge for half the existing volume. Consequently, the existing Menindee outlet regulator storage volume versus discharge relationship was adjusted to cater for this as shown in Figure 6.

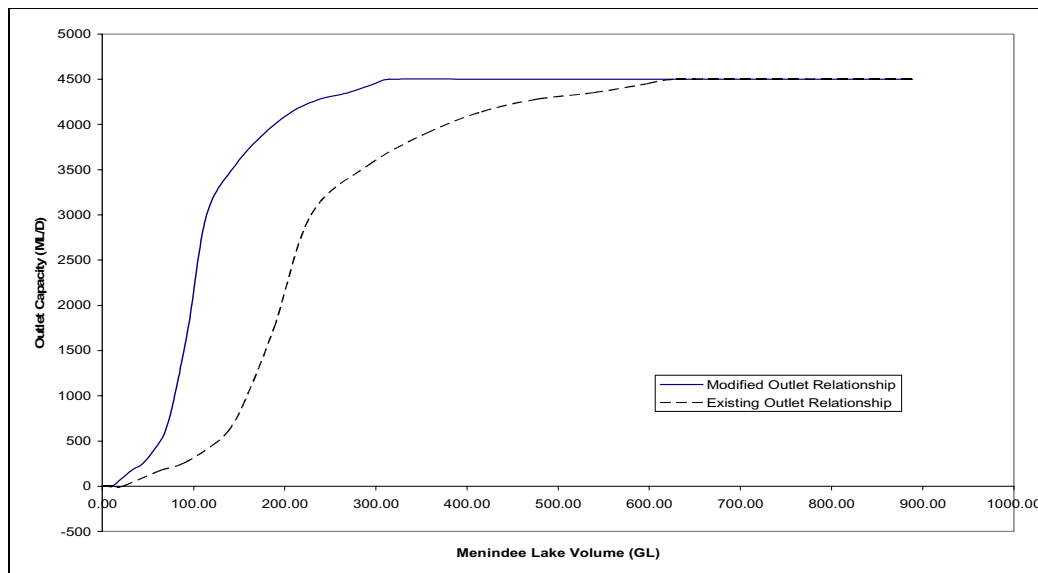


Figure 6 – Existing and Adjusted Menindee Outlet Capacity Relationship

3.2.7 Construction of a Two Menindee Lake Cells (One Filled)

Under this option only the half of Lake Menindee is used to store water, whilst the other half is restored to a more natural cycle of wetting and drying. The option still involves the construction of two cells, with the cell that is connected to Lake Cawndilla via Morton Boolka being filled.

3.2.8 Increasing the Capacity of Lake Pamamaroo

With appropriate target storage operation, creation of additional storage capacity in Lake Pamamaroo has the potential to reduce storage volume and storage durations in the more inefficient lakes. In modelling this option it was assumed that filling of Lake Pamamaroo to its new full supply level utilised the existing lakes filling sequence.

In increasing the lake capacity, the surcharge level of Lake Pamamaroo was raised by 0.8 meter to give a total capacity at an RL of 62.3 metres of 390 Gigalitres. This represents an increase in Lake Pamamaroo capacity of approximately 40 Gigalitres. Filling of this additional storage was achieved in the model through surcharging of Lake Wetherell. This surcharging increases the capacity of Lake Wetherell from 195 to 262 Gigalitres. In increasing the capacity of Lake Pamamaroo, the surface area was assumed to remain unchanged from the existing full supply level.

In modelling this option, the Pamamaroo regulator outlet capacity was increased in recognition of the additional available head created through increased lake capacity.

3.2.9 Potential Water Savings from Privately Owned Storages

As indicated in Table 1, the evaporative losses associated with off river dams such as ring tanks are quite large in comparison to major dams. A number of preliminary modelled case studies in the Namoi Valley were undertaken to assess potential water saving strategies from reduced evaporation from off-river storages. These consisted of:

- i) Purchasing all supplementary water licenses. Supplementary water is unregulated water in excess of releases from Keepit and Split Rock Dams.
- ii) Removal of all off-river storages and increasing storage capacity in Keepit and Split Rock Dams. Capacities for Split Rock and Keepit Dams were increased to 1,000 Gigalitres each.
- iii) Stopping of evaporation from on farm storage through surface covering.

3.3 Description of Non-Modelled Water Saving Options

3.3.1 General

As stated in Section 3.1, some options cannot be modelled, but still require assessment with respect to potential water savings. Key non modelled options for which potential water savings have been assessed using observed data on flows, losses and infrastructure performance are:

Key Non Modelled Options

- Improved extraction from residual pools in the Menindee Lakes Scheme.
- Improved use of existing smaller deeper lakes in the Menindee Lakes Scheme.
- Utilisation of existing and new storages upstream of the Menindee Lakes Scheme.
- Utilisation of existing and new storages downstream of the Menindee Lakes Scheme.

3.3.2 Improved Extraction from Residual Pools

The current distribution of residual storage in the Menindee Scheme is presented in Table 4.

Table 4 – Advised Residual Storage Volumes

Dead Storages	RL (m)	Residual Volume (ML)
Lake Balaka	61.50	1,200
Lake Malta	61.75	350
Lake Bijjie	61.00	900
Lake Tandure	57.80	9,448
Lake Wetherell	52.50	478
Lake Wetherell Total		12,376
Lake Pamamaroo	56.50	28,930
Lake Copi Hollow	58.35	2,800
Lake Pamamaroo Total		31,730
Lake Menindee	56.00	60,860
Lake Speculation	59.50	10,330
Lake Cawndilla	54.50	100,970
Total Residual Storage		216,266

As discussed in section 3.2.2 differences exist between the residual storage volume assumed in the modelled base case and the volume provided by DNR. In addition, the modelled frequency of access to residual pools is also likely to be different to that which is observed in practice. Any calculation of saving volumes and strategies will need to recognise these two issues.

An indication of the frequency of time that each lake spends in the residual pool zone based on the advised pool volumes and model results is shown in Figures 7. As can be seen, all lakes are above the residual pool zone for the majority of time.

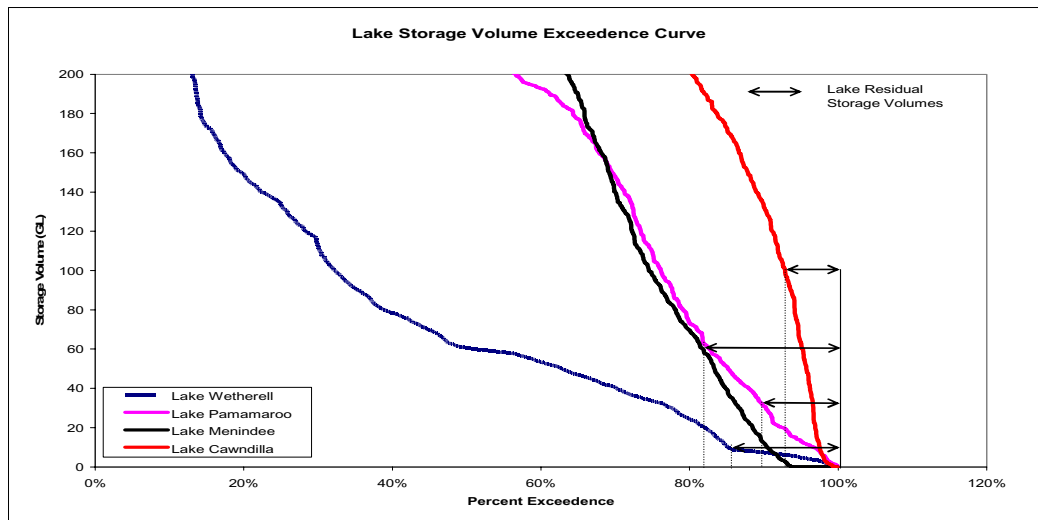


Figure 7 – Frequency of Lake Residual Storage Volume Exceedence

Improved access to residual storage volumes is likely to deliver only small long-term water savings. However, the years in which access takes place are drought years

therefore the importance of these volumes cannot be understated. An approximate indication of when these opportunities arise can be seen from the variation in total scheme volume over the long-term. This is shown in Figure 8.

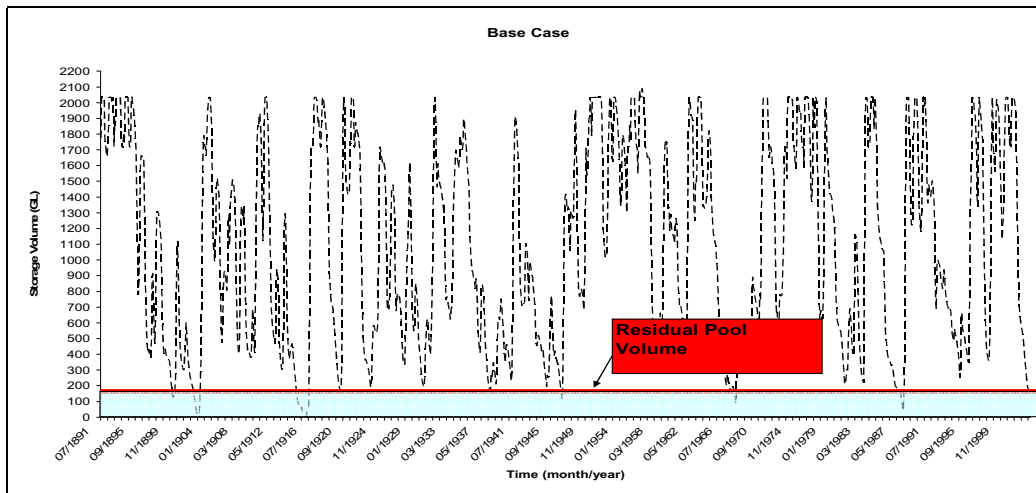


Figure 8 – Approximate Opportunities for Residual Pumping Over Time

3.3.3 Improved Use of Existing Smaller Deeper Lakes

There are a number of smaller lakes with the Menindee scheme that may be utilised more efficiently, through surcharging or increasing capacity. Use of these smaller deeper lakes as opposed to the wide shallow main lakes in times of low volumes and high demands may result in small water savings.

3.3.4 Use or Creation of Upstream Storage Capacity

Instream in The Upper Darling and Floodplain Storage at Menindee

An evaluation of the potential instream storage capacity in the Darling River above Menindee was undertaken using channel capacity and longitudinal survey section information for the Darling River.

An assessment of the volume of available storage resulting from the raising of Bourke Weir was made. Bourke was selected as information on channel cross section and longitudinal profile was available. In reality implementation of an instream storage option may need to occur closer to the Menindee Scheme to ensure that water can be moved from the inefficient lakes into the instream storage in times of drought operation. It is likely that the instream storage characteristics will remain unchanged.

The variation of storage volume with weir crest height is presented in Table 5. Construction of an impoundment with a crest level approaching the top of bank with a suitable regulator will lead to creation of 46 Gegalitres of storage occupying a surface area of 2,676 Ha. The weir pool will extend 200 kilometres upstream to Brewarrina.

Table 5 – Bourke Instream Storage

Comment	Crest Level (m)	Channel Area (Sqm)	Volume (GL)	Weir Pool Length (Km)	Surface Area (Ha)
Current Weir Hgt	4.9	168	4.8	86	443
	5	173	5.1	88	459
	6	227	8	105.6	591
	9	411	22	158.4	1077
Top Of Bank	12	652	46	211.2	2677

From a water saving perspective the small surface area of this additional storage offers advantages over the storing of an equivalent volume in the shallower more expansive Menindee Lakes.

Given that instream storage only offers small additional volumes, creation of additional floodplain storage in the immediate vicinity of the scheme to complement this instream storage was also assessed. In order for floodplain storage to be efficient, storages have to be deep. Typical ring tank depths are in the order of 3 metres, with depths to 6 metres also possible. The equivalent ring tank surface area for 150 Gigalitre of instream storage is presented in Table 6 for ring tank storages of 3 metres to 6 metres depth.

Table 6 – Bourke Ring Tank Storage

Storage Depth (m)	Surface Area (Ha)
3m	5,000
4m	3,750
5m	3,000
6m	2,500

Use of Existing Tributary Storages

The storage of water in dry times in existing or enlarged upstream storages in the New South Wales tributaries of the Darling as opposed to Menindee Lakes potentially offers water savings through reductions in evaporative losses. As discussed in Section 1.1 and shown in Table 1 upstream major dams have considerably less evaporation than that of the Menindee Scheme.

However, only a limited number of upstream storages can be used to supply Lower Darling water users. Limitations are primarily due to channel capacity constraints or the large flow reductions caused by flows passing through terminal wetlands. On the basis of this and discussions with NSW State Water staff, possible locations for storage and supply of Lower Darling volumes are :

- Keepit Dam on the Namoi River,
- Chaffey Dam on the Peel River,
- Pindari Dam on the Macintyre River.

Based on Table 1, it is likely the losses associated with evaporation will be considerably less than those at Menindee. However, this saving in volume may be potentially offset by the losses associated with delivering volumes to the Lower Darling. This is especially the case if delivery takes place during the summer months after a prolonged period of low to no flows.

It is important to note that delivery “losses” may have some environmental benefit. This should be borne when evaluating the relative merits of water savings strategies at the Menindee Scheme and upstream.

In order to gain an appreciation of the size of the losses associated with delivery of water from tributary storages to the Lower Darling, an analysis of the losses associated with small flow event releases Keepit Dam along the Namoi and Barwon Darling river systems has been undertaken.

Small flow events, at times when there is negligible irrigation extraction and ungauged tributary inflow are rare. Consequently, only a limited number of events were available for the analysis.

3.3.5 Use or Creation of Downstream Storage Capacity

Instream Storage in the Lower Darling

An evaluation of the potential instream storage capacity in the Darling River below Menindee was undertaken using channel capacity and longitudinal survey section information for the Darling River.

An assessment of the volume of available storage resulting from the raising of Burtundy weir was made. The variation of storage volume with weir crest height is presented in Table 7. Construction of an impoundment with a crest level approaching the top of bank with a suitable regulator will lead to creation of only 5 Gigalitres of storage with a surface area of 400Ha. The weir pool extends approximately 80 kilometres upstream.

Table 7– Burtundy In-stream Storage

Comment	Crest Level (m)	Channel Area (sqm)	Volume (GL)	Weir Pool Length (Km)	Surface Area (Ha)
Current Weir Hgt	1	6.5	0.0	17.6	37.4
	2	37	0.4	35.2	122.1
	3	74	1.3	52.8	209.9
	4	116	2.7	70.4	309.1
Top Of Bank	5	162	4.7	88	414.4

Instream Storage in the Murray

There is potential to store a volume of water through utilisation and enhancement of the existing Locks on the Murray River downstream of Wentworth. Use of this storage may mitigate the impacts of reduced storage volumes at the Menindee Lakes Scheme.

The locks are currently operated in non flood times to maintain a fixed river level irrespective of flow. There is the potential to vary the operation of the locks to increase the instream storage downstream of Menindee. A one metre increase in water level at each lock equates to approximately 100GL. Varying the water levels in each of the locks is likely to have environmental benefits if the variation mimics some aspects of the natural behaviour. There is also potential for storage at Chowilla or surcharging the existing lakes

4 DISCUSSION OF MODELLED RESULTS

4.1 General

Detailed results for each key modelled option are included in the Appendices to this report. In the following sections, summaries of evaporative savings, together with diversion, flow and salinity changes are presented. The following nomenclature has been adopted for describing modelled water savings options that have their genesis at the Menindee Lakes Scheme.

Base Case	The base case (current operation and development)
M0	Rapid emptying of the Scheme in the range of 480GL to 200GL
M1	Rapid emptying of the Scheme in the range of 480GL to 300GL
M2	Rapid emptying of the Scheme in the range of 680GL to 100GL
M3	Rapid emptying of the Scheme in the range of 300GL to 100GL
NoMC	More natural wetting and drying of Lake Menindee and Lake Cawndilla
NoCExMO	More natural wetting and drying of Lake Cawndilla
NoCEnMO	More natural wetting and drying of Lake Cawndilla
NoMExCO	More natural wetting and drying of Lake Menindee
NoMEnCO	More natural wetting and drying of Lake Menindee
MCell	Construction of two Menindee Lake cells
0.5M	Construction of a two Menindee Lake cells (One Filled)
PInc	Increasing the capacity of Lake Pamamaroo

4.2 Menindee Scheme - Potential Evaporative Savings

Evaporative savings for each of the key modelled options are presented in Table 8. The time series variation of evaporation for each option with respect to the base case is presented in Appendix 1. In recognition that the importance of evaporative losses is a function of the volume available in storage, the variation of evaporation volume as a proportion of the average annual storage volume is presented in Appendix 2 for each option.

Table 8 – Key Modelled Options - Evaporative Savings (GL/Yr)

Option	Wetherell Net Evap	Pamamaroo Net Evap	Menindee Net Evap	Cawndilla Net Evap	Total Net Evap (GL/Yr)	Decrease From Base Case (GL/Yr)
Base case	50	82	168	126	426	0
M0	62	77	128	105	372	-54
M1	64	81	133	108	387	-39
M2	55	69	117	95	335	-91
M3	69	81	143	113	406	-20
NoMC	117	94	5	0	215	-211
NoCExMO	80	91	183	0	353	-73
NoCEnMO	82	92	176	0	351	-76
0.5M	56	84	87	130	357	-70
NoMExCO	75	83	0	134	291	-136
NoMEnCO	83	92	0	118	292	-134
PInc	65	86	162	123	435	+9
MCell	50	82	130	123	388	-38

All but one of the key modelled options produces evaporative water savings. The exception is the Pamamaroo increased capacity option in which the savings created by increased storage in Lake Pamamaroo is more than offset by the additional evaporative losses incurred in Lake Wetherell. This is a consequence of Lake Wetherell storage volumes and inundated areas having to be increased in order to fill Lake Pamamaroo.

Restoration of Lake Menindee and Cawndilla to more natural cycles of wetting and drying result in the largest evaporative saving of any option. This is followed by restoration of Lake Menindee only. As discussed previously use of these Lakes for flood mitigation purposes would reduce these saving volumes.

Options which seek to increase the release rate from the lakes when in New South Wales control, and thereby reduce the time that water spends within the scheme also produce substantial savings. In general approximately 100 to 200 Megalitres per annum is saved for every Gigalitre of water that remains in New South Wales control below 680 Gigalitres.

A number of savings options have been assessed with differing regulator outlet capacity configurations. This was undertaken in an effort to ensure that downstream demand could still be met on a daily basis. These options produced almost negligible change in the evaporative savings volumes. This is thought to be due to the modelled target storage operation remaining unchanged from the base case, and the times when demands avail of this additional capacity being infrequent.

There is potentially some scope to for further efficiency gains through optimising scheme operation for each of the modelled options. However, changing the assumed target storage operation within the model in order to better utilise the lakes for each water saving option requires modification to the source code within MSM. This was not possible as a consequence of the short study timeframes. However, this should be addressed during the more detailed second phase of the project.

4.3 Consequences of Menindee Scheme Savings

4.3.1 Longterm Average Diversion Change and Reliability

Any option that seeks to reduce the storage time or storage volume within the lake scheme is going to result in changes to average downstream diversions and reliability. Impacts on average diversions for each option are presented in Table 9. Changes in both the magnitude of peak shortfalls and their frequency are presented in Appendix 3 as part of the summary outputs for each option. Exceedence curves of changes in the Lower Darling, and New South Wales, Victorian and South Australian Murray Diversions are presented in Appendix 4. Time series of annual diversions are presented in Appendix 5.

Modelled options produce substantially larger average and inter year impacts upon Lower Darling Diversions than for Murray River Diversions. In general, average and inter year diversions for New South Wales, Victorian and South Australian Murray users are only altered by small amounts. The largest impact on Lower Darling average diversions is for the restoration of both Menindee and Cawndilla to more natural cycles of wetting and drying. This option result in average diversion reductions in the New South Wales Lower Darling of 74%. The restoration of Lake Cawndilla to more natural wetting and drying also results in a substantial decrease in

Lower Darling average diversions (53%) and increased spells of diversion shortfall years. This can be seen in the time series plots of annual diversions in Appendix 5. The option with the least impact on diversions and reliability is the construction of two cells in Lake Menindee.

Table 9 – Longterm Average Diversion Change (GL/Yr)

Year	Total NSW Lower Darling Div (GL/Yr)	Decrease from Base Case (GL/Yr)	Total NSW Murray Div (GL/Yr)	Decrease from Base Case (GL/Yr)	Total Vic Murray Div (GL/Yr)	Decrease from Base Case (GL/Yr)	Total SA Murray Div (GL/Yr)	Decrease from Base Case (GL/Yr)
Base case	129		1966	0	1675		1139	
M0	119	-10	1979	13	1671	-4	1143	4
M1	121	-8	1986	20	1674	-1	1143	4
M2	112	-17	1969	3	1665	-10	1145	6
M3	124	-5	1979	13	1673	-2	1144	5
NoMC	32	-97	1922	-44	1636	-39	1141	2
NoCExMO	55	-74	1968	3	1670	-5	1142	3
NoCEnMO	55	-74	1969	3	1671	-4	1142	3
0.5M	116	-13	1968	2	1675	0	1142	3
NoMExCO	116	-13	1963	-2	1673	-2	1142	3
NoMEnCO	112	-17	1964	-2	1672	-3	1143	4
PInc	122	-7	1966	0	1675	0	1140	1
MCell	129	0	1966	0	1675	0	1139	0

4.3.2 Flow Change

Flow changes resulting from key modelled options are presented in Tables 10 and 11. Specific examples of flow regime changes in the Darling at Wentworth and the Murray at Lock 7 are presented in the form of flow duration curves in Figures 9 and 10.

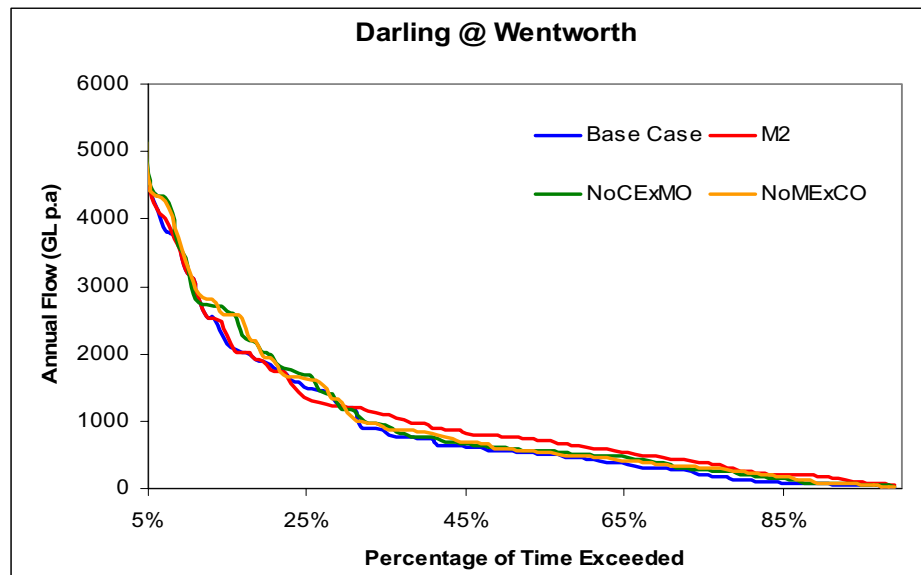


Figure 9 – Annual Flow Exceedence Curve (Darling River @ Wentworth)

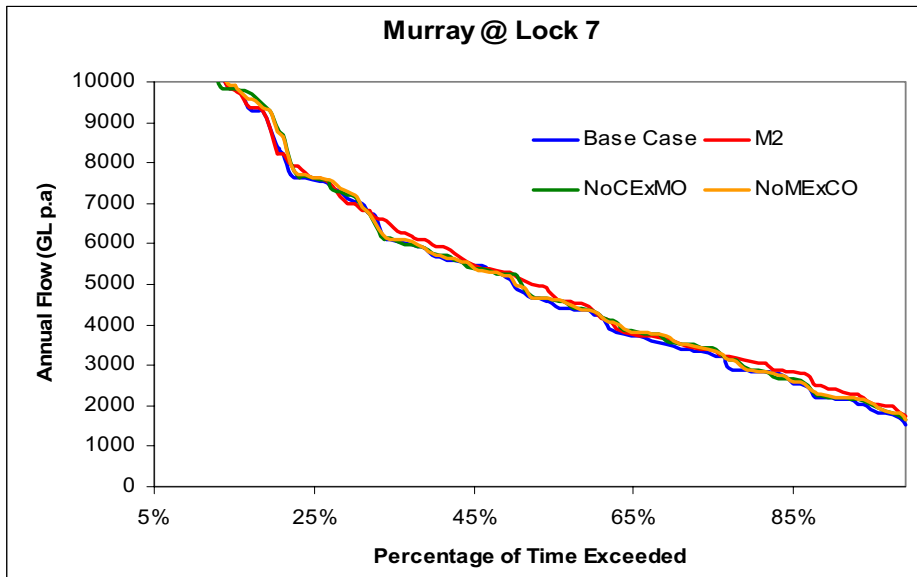


Figure 10 - Annual Flow Exceedence Curve (Murray River @ Lock 7)

With the exception of the option of increased capacity of Pamamaroo, all options produce increased flows in the Lower Darling. Most options also reduce the volume of flow released and spilt from Lake Cawndilla. The exception is the option in which the Cawndilla outlet is enlarged. Under this option Cawndilla releases increase by 98 Gialitres per annum.

Flows in the Murray upstream of Wentworth are largely unchanged by water saving options at Menindee. Although restoring Lakes Menindee and Cawndilla to natural wetting and drying cycles results in increases in Murray flows upstream of Wentworth of approximately 80 Gialitres per annum.

Flows downstream of Wentworth generally increase in most options. This results in increased spills from Lake Victoria and a corresponding reduction in regulated releases. Flow across the South Australian border also increases.

An example of the variability of flows with respect to time for both the base case and the restoration of Lake Menindee too a more natural regime is shown in Figures 11 to 13. Further examples of the alteration to flow regimes for additional options are presented in Appendix 6. Options generally increase the frequency of over bank events in the Lower Darling but result in only minor changes in the Murray River flow regime.

It should be noted that the distribution of flows within the Anabranh or outflows from the Anabranh are not simulated in the version of MSM used for the first stage of this project. Refinement of options in further stages of this project should incorporate a more detailed analysis of Anabranh flows.

Table 10 – Average Annual Flows (GL/Yr)

	Base Case	NoMC	PCI	0.5M	NoCExMO	NoCEnMO	NoMExCO	NoMEnCO	MO	M1	M2	M3
Lake Cawndilla Release (GL/Yr)	139	0	134	132	0	0	104	237	110	113	103	118
Lake Cawndilla Spill (GL/Yr)	11	0	0	18	0	0	0	0	11	11	10	11
Weir 32 Flow (GL/Yr)	1671	1968	1670	1751	1815	1817	1812	1817	1735	1718	1780	1697
Burtundy Flow (GL/Yr)	1158	1333	1144	1209	1235	1237	1241	1246	1223	1206	1268	1186
Darling U/S Wentworth (GL/Yr)	1140	1315	1126	1191	1217	1219	1223	1228	1205	1188	1250	1168
Murray U/S Wentworth (GL/Yr)	6062	6144	6062	6061	6066	6065	6068	6068	6055	6047	6070	6053
Lake Victoria Spill (GL/Yr)	4218	4867	4209	4324	4494	4495	4700	4705	4317	4287	4390	4253
Lake Victoria Release (GL/Yr)	248	232	244	230	207	206	195	188	242	250	238	251
Lock 7 (GL/Yr)	6460	6704	6447	6505	6533	6534	6541	6545	6516	6492	6576	6479

Table 11 – Increases in Average Annual Flows from Base Case

	NoMC	PCI	0.5M	NoCExMO	NoCEnMO	NoMExCO	NoMEnCO	MO	M1	M2	M3
Lake Cawndilla Release (GL/Yr)	-139	-5	-7	-139	-139	-35	98	-29	-26	-36	-21
Cawndilla Spill (GL/Yr)	-11	-11	7	-11	-11	-11	-11	0	0	-1	0
Weir 32 Flow (GL/Yr)	297	-1	80	144	146	141	146	64	47	109	26
Burtundy Flow (GL/Yr)	175	-14	51	77	79	83	88	65	48	110	28
Darling U/S Wentworth	175	-14	51	77	79	83	88	65	48	110	28
Murray U/S Wentworth	82	0	-1	4	3	6	6	-7	-15	8	-9
Lake Victoria Spill	649	-9	106	276	277	482	487	99	69	172	35
Lake Victoria Release	-16	-4	-18	-41	-42	-53	-60	-6	2	-10	3
Lock 7 Flow (GL/Yr)	244	-13	45	73	74	81	85	56	32	116	19
Evaporative Saving At Menindee (GL/Yr)	211	-9	70	73	76	136	134	54	39	91	

Base Case

NoMExCo

	Jul	Aug	Sep	Oct	Nov	Dec	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Jan	Feb	Mar	Apr	May	Jun
189192	16700	16000	20367	27433	30900	25735	17367	9167	1867	167	233	367	18300	18967	21533	27400	31167	26200	15000	6567	1167	167	233	367
189293	533	5300	5800	6100	11900	16367	17600	15833	10667	12767	18167	19367	5133	7500	6067	6367	11967	16633	18300	12433	11200	15233	18767	20033
189394	20100	21133	27967	34500	31167	20967	11767	4233	767	2767	11933	19033	20000	21167	28067	34733	31533	20900	8300	2467	833	6933	14500	19433
189495	20100	24133	22733	18533	14433	13500	5667	833	1200	2833	1800	467	21233	24133	22700	18633	12833	9800	4067	1233	7567	8667	17333	167
189596	467	433	400	200	4367	7667	7467	3000	233	233	200	200	167	167	133	67	1167	4767	4733	4467	2033	2533	2633	800
189697	167	167	133	100	6233	8667	4967	3200	1167	200	200	167	167	167	133	4867	5900	3367	2467	2267	1000	200	200	167
189798	200	267	267	167	5667	7033	3400	1000	467	233	200	167	167	200	267	133	5033	7333	4900	4967	2000	2567	1633	167
189899	167	167	133	100	4600	5667	2767	800	233	267	200	167	167	167	133	100	4533	4433	2067	1033	367	267	200	167
189900	167	167	100	100	133	67	167	167	33	167	200	200	167	267	233	133	133	67	167	133	0	167	200	200
190001	167	200	133	100	2867	5700	3933	1100	233	167	33	-33	167	200	867	567	2833	6033	4200	1900	767	233	100	0
190102	0	133	167	100	67	67	133	233	233	200	200	-133	0	233	300	133	2467	1633	133	233	233	200	200	133
190203	167	167	133	100	67	67	-33	-67	-67	-67	100	167	133	167	133	67	-67	-67	-100	-67	-67	-67	100	167
190304	167	167	133	133	9167	15567	13233	4500	300	200	367	467	167	167	1067	8133	14533	17167	12767	4200	467	1167	4300	3267
190405	1500	2267	2200	1067	1833	6167	7500	2900	233	300	233	233	2800	3533	3067	1167	100	5067	5767	1833	233	200	300	233
190506	167	300	233	100	4467	6900	5000	2233	667	233	233	200	233	300	233	100	3500	4833	2767	1067	467	233	233	200
190607	167	300	300	133	167	133	3467	2300	1033	800	200	200	167	200	167	100	3433	2433	3267	3633	3200	2200	1533	800
190708	167	333	267	5100	7100	4933	2267	633	233	233	233	200	167	333	233	4633	5000	2700	1667	700	233	1400	3500	2300
190809	167	333	267	133	5000	6867	4733	1700	267	267	233	233	447	200	133	133	4633	6167	3800	1000	633	267	233	200
190910	167	167	133	100	633	2267	1400	200	333	233	233	200	167	300	267	133	633	3567	2200	833	3867	5067	7467	3800
191011	367	467	433	367	367	5167	7867	3167	1933	10333	10833	3067	767	3000	2167	367	167	4733	4167	667	8367	15200	11567	2700
191112	500	600	500	4667	7733	5600	5667	2933	233	233	200	167	267	167	133	1367	5133	4367	2633	1733	533	0	0	0
191213	167	200	133	100	233	3767	3733	1067	333	167	100	133	0	100	133	100	233	3767	3767	1100	333	167	100	100
191314	167	200	133	100	233	4100	3200	3633	267	267	233	200	133	167	3533	4667	467	1467	2667	1467	267	233	233	200
191415	167	200	133	100	167	167	133	233	233	200	133	33	167	133	100	100	167	167	133	233	233	233	133	67
191516	0	0	67	100	-67	-67	-100	-67	-67	67	200	200	0	33	167	167	0	-67	-100	-67	-67	33	167	200
191617	200	200	200	267	5100	7067	9167	12833	10533	12100	9333	2100	200	200	2033	10200	10833	7033	8967	12667	14833	15433	9600	1967
191718	500	633	533	400	8100	11633	13067	15333	9167	2533	867	500	200	200	167	133	6367	9467	12600	16267	14167	4867	767	200
191819	433	467	400	200	100	5067	8000	3200	233	233	267	200	167	167	133	100	100	4233	4200	2067	800	233	267	133
191920	167	200	133	100	133	167	133	233	233	200	167	167	0	67	67	67	67	67	67	67	67	67	67	67
192021	67	267	8333	16000	16400	13900	7900	2333	300	300	233	233	67	8900	16167	18567	17500	8433	4967	2967	300	233	200	200
192122	2000	11467	19767	25133	33833	23000	14767	10800	3733	267	200	200	5767	13800	20100	26867	33967	22933	10033	7800	6967	2200	200	200
192223	167	167	100	1067	5700	7933	6033	3433	1067	200	200	200	167	167	100	100	4500	4433	2033	967	167	-67	0	0
192324	167	67	0	67	133	100	-100	-33	267	200	167	0	0	67	33	33	133	100	-100	-33	233	267	200	167
192425	167	167	133	100	167	200	767	600	233	233	200	167	133	167	133	100	167	167	6233	6267	967	233	233	200
192526	200	333	233	100	3100	6967	8800	2667	267	200	200	167	200	200	133	100	167	4633	4500	4500	2233	200	267	200
192627	167	300	233	100	100	5067	6733	2433	233	233	200	167	2067	1633	333	100	100	4833	4967	2267	800	233	200	167
192728	167	267	267	1833	1200	133	167	267	267	233	200	167	167	267	233	1967	1300	133	167	267	267	233	200	167
192829	200	133	100	2967	2833	5600	6467	2267	233	267	200	133	200	3833	6400	2800	200	4967	4967	2267	867	233	200	133
192930	167	267	267	2667	1800	200	167	233	100	100	67	67	167	267	233	2800	1867	200	167	233	233	233	200	200
193031	133	200	133	100	167	133	100	167	233	233	200	167	167	200	167	200	167	200	1600	300	333	233	200	167
193132	167	8667	15200	11267	5300	5967	7800	3400	267	300	233	200	5933	13567	18200	13500	3100	2700	6733	3400	267	300	233	200
193233	167	167	167	100	167	4800	5000	1433	233	267	200	167	167	167	167	100	167	4133	4300	1233	233	267	200	167
193334	167	267	267	133	1300	1167	5267	3333	233	267	200	133	167	267	267	133	1300	1300	6967	5200	3233	2633	700	133
193435	167	167	133	300	1767	28967	1333	3200	2166	300	367	433	167	167	100	2800	3900	3533	3000	3733	2500	200	167	167
193536	467	433	233	133	133	4233	2867	200	233	233	200	167	167	300	233	133	133	2867	2033	200	233	233	200	167
193637	200	167	167	100	1567	3233	1800	200	233	200	200	167	167	167	167	100	100	100	1033	267	200	233	200	167
193738	167	267	267	2600	1767	133	133	167	167	133	0	67	167	267	267	3267	2067	133	133	233	200	233	167	133
193839	200	167	100	167	67	100	100	300	267	233	200	167	200	167	100	167	67	67	100	300	300	267	233	200
193940	167	167	133	133	200	133	667	667	200	300	200	167	167	267	267	167	200	133	2267	1567	200	300	200	167
194041	167	167	100	67	133	100	267	1433	1067	233	367	467	1											

Base Case

NoMExCO

	Aug	Sep	Oct	Nov	Dec	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Jan	Feb	Mar	Apr	May	Jun	Jul	
189192	4113	6087	7127	6403	4490	2913	1767	1087	930	750	620	600	4113	6087	7127	6403	4490	2913	1767	1087	930	750	620	600	
189293	1373	2347	3083	2967	2400	2153	1783	1087	1100	1587	2077	3070	2037	2767	3123	2623	2487	2167	1850	1200	1133	1823	2747	4023	
189394	4840	5967	6460	7120	6423	3650	1450	927	900	750	2800	4410	4840	5967	6470	7140	6450	3647	1120	647	620	1483	3100	4453	
189495	5393	6983	8250	10183	10987	7490	1923	927	900	750	620	600	5480	6987	8250	10190	10847	7193	1753	847	723	1130	1033	827	
189596	8167	18900	2583	1757	900	807	723	647	620	710	620	600	13167	18833	25533	17467	800	723	723	647	620	4500	5900	9100	
189697	6700	7333	7500	8000	8433	7233	6467	6200	4500	3100	3000	3000	6900	7500	4900	5700	8000	7233	7233	6467	6200	4500	3100	3000	
189798	3633	4300	4400	4100	5000	7233	6467	6200	4500	3100	3000	3000	3633	4133	13133	6947	8000	7233	7233	6467	6200	4500	3100	3000	
189899	3633	13033	14133	6167	6000	7233	6467	6200	4500	3100	3000	3000	9800	14100	14133	6167	6000	7233	7233	6467	6200	4500	3100	3000	
189900	18700	14967	8533	5700	6000	7233	6467	6200	4500	3100	3000	13967	18700	15067	8633	5700	6000	7233	7233	6467	6200	4500	3100	13967	
190001	23600	33033	34800	18767	6000	7233	6467	6200	4500	3100	2967	2967	23600	33033	35300	19300	6000	7233	7233	6467	6200	4500	3100	2967	
190102	3967	6767	17433	13967	3800	7233	6467	6200	4500	3100	2967	2967	3967	6767	17633	13967	3800	7233	7233	6467	6200	4500	3100	2967	
190203	3300	2967	2633	2933	3300	3900	4267	4267	4333	4000	3100	3167	3400	2633	2633	3400	3800	4533	4900	4500	4733	4233	3100	2733	
190304	18900	18900	18900	12333	12333	17000	16100	8133	6000	4500	3100	3000	17233	18900	17767	20967	18900	18933	15700	7833	6000	4500	3100	7833	
190405	13000	26533	22867	15100	7833	9667	7233	6467	6200	4500	3887	8333	18833	27833	22667	14167	5767	7233	7233	6467	6200	4500	3100	8000	
190506	25200	31967	20100	8267	6467	7233	6467	6200	4500	3100	14267	25267	31967	20100	8233	5300	7233	7233	6467	6200	4500	3100	8000	14267	
190607	30433	38200	42700	51933	59533	33367	7233	6900	9300	7500	6200	3000	30467	38133	42733	52300	63067	35900	7233	6467	6200	4500	3100	7467	
190708	3633	4133	7500	6400	6000	7233	6467	6200	4500	3100	3000	3000	7867	10333	8867	5700	8000	7233	7233	6467	6200	4500	3100	3000	
190809	3633	5367	12100	8167	6333	7233	6467	6200	4500	3100	2967	2967	3633	5067	12000	8167	6000	7233	7233	6467	6200	4500	3100	2967	
190910	30400	38733	47867	34133	6000	7233	6467	6200	4500	3100	3000	3000	30400	38800	47967	34167	6000	7233	7233	6467	6200	4500	3100	1267	
191011	6733	8900	28300	27233	11000	10333	8067	10800	9000	10733	16933	24867	13733	18600	28100	27300	10600	7233	7233	8500	12667	18300	17800	24567	
191112	29000	29000	14867	8800	7900	7233	6467	6200	4500	3100	3000	3000	29067	28567	14467	5700	6000	7233	7233	6467	6200	4500	3100	3000	
191213	6767	10933	20700	11433	6167	7233	6467	6200	4500	3887	7500	3633	6767	10967	20667	11433	6133	7233	7233	6467	6200	4500	3400	7500	
191314	7700	8200	8200	8200	8200	7233	6467	6200	4500	3100	3000	3000	7700	8200	8200	8200	8200	7233	7233	6467	6200	4500	3100	3000	
191415	3633	3733	4033	5000	5333	6500	6667	8133	8100	4500	3100	2833	3633	3700	4000	4967	5300	6467	6067	6033	4500	3100	2867	3000	
191516	19233	29133	32433	29833	10733	6800	7233	6467	6200	4500	3100	2833	19233	29167	32500	29900	10767	6833	7233	6467	6200	4500	3100	2867	
191617	14433	32733	41400	49400	59967	57467	37233	22333	14067	15233	14067	15233	14967	32733	42733	56867	65400	57967	37267	22200	18100	18633	20200	35233	
191718	5533	90400	12867	16267	18133	144000	57033	24300	14233	7933	25433	36000	5533	90333	128667	165933	183333	142433	25067	19000	10400	25467	35667	35767	
191819	46933	59167	64533	53167	15933	9967	7233	6467	6200	4500	3100	3000	46700	59900	64700	53067	15933	7233	7233	6467	6200	4500	3100	3000	
191920	7000	8467	7233	6467	6200	4500	3100	3000	3000	3000	3000	3000	7000	8467	7233	6467	6200	4500	3100	3000	3000	3000	3000	3000	
192021	9667	29667	44300	52433	38533	20700	10333	9267	9000	7500	6200	3000	9900	35900	50033	55100	39633	15967	7233	6467	6200	4500	3100	16333	
192122	15633	37933	52267	62000	59533	30100	15900	11900	9000	7500	6200	6000	23633	39833	52767	63400	58367	30167	10733	8767	7067	4500	5633	8833	
192223	6733	7233	15267	8800	8367	7233	6467	6200	4500	3100	6367	7900	13200	18000	7900	6000	7233	7233	6467	6200	4500	3100	6367	6367	
192324	29333	39867	40333	33367	20000	7767	7233	6467	6200	4500	3100	3000	29767	39867	40333	33367	19833	5000	7233	6467	6200	4500	3100	5633	
192425	8000	17867	30667	37133	34567	11433	9267	9000	7500	6200	3000	3000	8833	13200	30833	35733	39333	32000	20900	13233	6200	4500	3100	11100	
192526	20033	30133	32467	22300	3767	7233	6467	6200	4500	12533	10733	10733	29167	30067	32667	22300	3767	7233	6467	6200	4500	3100	3000	19833	
192627	25067	33233	33633	31267	12633	7633	7233	6467	6200	4500	3100	3000	26967	34300	36967	31267	12633	7233	7233	6467	6200	4500	3100	3000	
192728	3633	4200	6600	5700	6000	7233	6467	6200	4500	5133	18733	3633	3633	4133	5567	5700	6000	7233	7233	6467	6200	4500	3100	18733	
192829	20133	12167	7500	8800	8500	7267	7233	6467	6200	4500	3100	6267	20133	15633	10633	11833	8000	7233	7233	6467	6200	4500	3100	6267	
192930	7900	6733	6300	5700	6000	7233	6467	6200	4500	3100	3000	3000	7900	6767	6300	5700	6000	7233	7233	6467	6200	4500	3100	3000	
193031	3633	4167	4200	4167	4200	4167	4200	4167	4200	4167	4200	4167	3633	4167	4200	4167	4200	4167	4200	4167	4200	4167	4200	4167	
193132	61633	67567	106400	74467	34300	10333	10333	9267	9000	7500	7467	22133	61633	67567	106400	74467	34300	10333	10333	9267	9000	7500	7467	15233	22133
193233	30733	39967	40300	38967	15967	7667	7233	6467	6200	4500	3100	3000	30733	39967	40333	38900	16000	7233	7233	6467	6200	4500	3100	3000	
193334	7233	18833	24533	12333	6000	7233	10067	9267	9000	7500	6200	5700	6500	18833	24533	12333	6000	7367	10167	8833	6000	7100	8033	5733	
193435	3633	3900	24667	36000	41233	44400	28933	9267	9000	7500	6200	18900	7967	10400	24967	39600	43000	49033	28233	9300	7467	9067	14100	16267	
193536	27800	39833	45767	46333	26233	8533	9000	9467	6200	4500	3100	3000	27500	39833	45767	46333	26233	7233	8133	6467	6200	4500	3100	3000	
193637	17867	32667	44433	6000	7233	6467	6200	4500	3100																

Base Case

NoMExCo

	Jul	Aug	Sep	Oct	Nov	Dec	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Jan	Feb	Mar	Apr	May	Jun
189192	28900	50333	67333	43067	15500	4300	1933	2733	2433	1867	5300	11267	28900	50333	67333	43067	15500	4300	1933	2733	2433	1867	5300	11267
189293	22633	21200	25900	20067	14700	7300	2567	2233	1667	4100	9500	23533	22633	21200	25900	20067	14700	7300	2567	2233	1667	4100	9500	23533
189394	33267	41200	44967	46333	40067	14400	3467	2833	3600	11767	18333	29533	33267	41200	44967	46333	40067	14400	3467	2833	3600	11767	18333	29533
189495	40567	54833	71533	99000	113167	67800	9667	4533	8600	5400	8933	8367	40567	54833	71533	99000	113167	67800	9667	4533	8600	5400	8933	8367
189596	13800	1967	2700	18633	5967	2600	1800	3767	4333	5500	9033	8600	13800	1967	2700	18633	5967	2600	1800	3767	4333	5500	9033	8600
189697	10467	7867	5767	2733	1733	3567	3400	3200	3800	4733	5700	10467	7867	5767	2733	1733	3567	3400	3200	3800	4733	5700	10467	7867
189798	7867	10787	16633	7300	2333	1467	1500	4133	2767	3533	7800	9700	7867	10787	16633	7300	2333	1467	1500	4133	2767	3533	7800	9700
189899	10367	14433	15100	7067	3133	3900	4300	5133	5700	8900	11200	10367	14433	15100	7067	3133	3900	4300	5133	5700	8900	11200	10367	14433
189900	19567	15367	9200	3767	2933	5500	6567	7400	9733	10700	11767	14200	19567	15367	9200	3767	2933	5500	6567	7400	9733	10700	11767	14200
190001	24667	34200	38200	19033	4500	1967	1700	2633	3533	5767	7967	7133	24667	34200	38200	19033	4500	1967	1700	2633	3533	5767	7967	7133
190102	8900	9633	18633	12733	5533	3900	4967	6267	8333	7533	5367	9400	8900	9633	18633	12733	5533	3900	4967	6267	8333	7533	5367	9400
190203	5333	3633	4267	3800	3000	4533	4267	5567	5967	5967	8533	8733	5333	3633	4267	3800	3000	4533	4267	5567	5967	5967	8533	8733
190304	20000	19167	17033	13133	5700	3700	5033	4733	3000	4133	3467	4933	20000	19167	17033	13133	5700	3700	5033	4733	3000	4133	3467	4933
190405	16733	25667	21600	15033	7667	3800	3967	3567	3533	3900	9033	8400	16733	25667	21600	15033	7667	3800	3967	3567	3533	3900	9033	8400
190506	26667	32933	20167	8633	4067	1867	1533	3333	7100	7733	6800	16600	26667	32933	20167	8633	4067	1867	1533	3333	7100	7733	6800	16600
190607	31800	40767	45567	58667	67200	31233	4033	2800	2100	3933	6667	7133	31800	40767	45567	58667	67200	31233	4033	2800	2100	3933	6667	7133
190708	8167	10700	7700	2767	2833	3533	2300	3767	3967	2900	6933	7533	8167	10700	7700	2767	2833	3533	2300	3767	3967	2900	6933	7533
190809	9167	9200	12467	8767	3233	2167	2700	4167	5600	6333	12167	20867	9167	9200	12467	8767	3233	2167	2700	4167	5600	6333	12167	20867
190910	31067	41367	52933	33133	5600	3467	5333	3833	5233	4533	5533	7467	31067	41367	52933	33133	5600	3467	5333	3833	5233	4533	5533	7467
191011	13500	16333	28900	28133	11167	4433	4267	9067	5900	4667	6600	22833	13500	16333	28900	28133	11167	4433	4267	9067	5900	4667	6600	22833
191112	29567	28100	14367	5200	2100	3467	2433	4000	4300	4300	5000	6600	29567	28100	14367	5200	2100	3467	2433	4000	4300	4300	5000	6600
191213	8733	11433	22067	12300	6767	5567	3800	4067	6333	6567	7800	8067	8733	11433	22067	12300	6767	5567	3800	4067	6333	6567	7800	8067
191314	6233	14067	2667	5300	1400	2667	7800	6200	4533	2600	44667	7067	6233	14067	2667	5300	1400	2667	7800	6200	4533	2600	44667	7067
191415	5967	3533	3967	2233	3967	8333	8233	4000	6100	7267	7400	8267	5967	3533	3967	2233	3967	8333	8233	4000	6100	7267	7400	8267
191516	20933	30233	33200	31000	11633	4500	5500	5400	3633	6100	7433	7100	20933	30233	33200	31000	11633	4500	5500	5400	3633	6100	7433	7100
191617	22133	33733	45133	54800	62333	56800	27233	9067	4700	4233	11100	35333	22133	33733	45133	54800	62333	56800	27233	9067	4700	4233	11100	35333
191718	63667	104267	150367	198733	210567	150167	40033	8000	6100	6100	25533	37733	63667	104267	150367	198733	210567	150167	40033	8000	6100	6100	25533	37733
191819	51900	66433	72567	58867	14033	2000	1500	4867	4300	4700	6833	7633	51900	66433	72567	58867	14033	2000	1500	4867	4300	4700	6833	7633
191920	8533	5900	4233	5200	3400	3400	4000	4000	4000	4000	4000	4000	8533	5900	4233	5200	3400	3400	4000	4000	4000	4000	4000	4000
192021	16233	29733	40200	42400	22333	7233	3133	4233	4833	4867	6500	11467	16233	29733	40200	42400	22333	7233	3133	4233	4833	4867	6500	11467
192122	19267	29633	39767	45500	28633	6133	2067	2633	1767	2633	6133	6933	19267	29633	39767	45500	28633	6133	2067	2633	1767	2633	6133	6933
192223	8267	14100	18967	8567	2467	2267	1433	2067	2333	3200	5967	15067	8267	14100	18967	8567	2467	2267	1433	2067	2333	3200	5967	15067
192324	32400	43133	42967	33800	20833	8867	5033	5400	6567	8233	9000	32400	43133	42967	33800	20833	8867	5033	5400	6567	8233	9000	32400	
192425	9433	19000	32500	39967	39967	36533	14500	6500	3733	2767	5500	13967	9433	19000	32500	39967	39967	36533	14500	6500	3733	2767	5500	13967
192526	29433	38000	33133	24000	6900	2033	1467	2400	3867	4900	17700	19633	29433	38000	33133	24000	6900	2033	1467	2400	3867	4900	17700	19633
192627	25800	34333	38600	32000	13467	4433	1733	2700	3733	2167	5133	6733	25800	34333	38600	32000	13467	4433	1733	2700	3733	2167	5133	6733
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192829	20400	12400	5167	10800	7500	2800	1433	2967	3667	7400	10133	8300	20400	12400	5167	10800	7500	2800	1433	2967	3667	7400	10133	8300
192930	8333	7233	7033	4533	4167	7100	4433	3000	3867	6800	8000	7400	8333	7233	7033	4533	4167	7100	4433	3000	3867	6800	8000	7400
193031	4967	41600	16033	6000	7000	10300	7800	10200	4533	2600	44667	10267	4967	41600	16033	6000	7000	10300	7800	10200	4533	2600	44667	10267
193132	71033	106333	104333	70067	25867	5500	2033	4433	5667	11700	15700	22633	71033	106333	104333	70067	25867	5500	2033	4433	5667	11700	15700	22633
193233	31633	38400	43400	41300	15700	4467	3233	2767	2267	2733	5600	7967	31633	38400	43400	41300	15700	4467	3233	2767	2267	2733	5600	7967
193334	13933	19367	25300	12867	5667	8200	5533	5367	4867	5567	8200	6000	13933	19367	25300	12867	5667	8200	5533	5367	4867	5567	8200	6000
193435	8900	17667	25900	35633	43967	47033	24633	5100	2900	6533	14963	18963	8900	17667	25900	35633	43967	47033	24633	5100	2900	6533	14963	18963
193536	28467	39233	50767	49867	29533	5633	3033	4567	4233	7767	7633	28467	39233	50767	49867	29533	5633	3033	4567	4233	7767	7633	28467	
193637	18967																							

4.3.3 Salinity

As water storage reduces during drought because of evaporation, surface water salinity increases with the concentration of salts. Salinity of the surface water in an extended drought may make it unsuitable for some irrigation, such as for horticulture, and the quality of water supplied may not be of the standard required, irrespective of availability of supply. Changes in the long term average and median end of month salinity concentrations resulting from each of the key modelled options are presented in Tables 12 to 15³. In some cases long term average salinity concentrations are biased by individual salinity readings. These high readings typically occur for very small lake volumes. In order to ensure that this did not unduly affect the conclusions with respect to salinity changes as a result of each option, salinity exceedence curves have been produced to compliment the results of Table 12 and 13. These can be found in Appendix 7.

Table 12 – Longterm Average End of Month Salinity (EC)

	ECWeth	ECPam	ECMen	ECCawn	ECw32	ECLowDarl	ECAnnab	ECusTandou
Base Case	376	616	1280	1604	429	418	378	602
M0	381	859	1581	2237	412	380	337	521
M1	380	771	1646	2032	414	389	354	550
M2	384	1129	1063	2038	403	351	293	448
M3	380	854	1298	2464	416	390	346	535
NoMC	385	1351	0	0	417	417	52	208
NoCExMO	376	448	1501	0	467	461	35	235
NoCEnMO	380	404	1567	0	432	432	34	217
0.5M	370	573	1411	952	417	408	351	559
NoMExCO	375	715	435	868	389	370	384	543
NoMEnCO	381	438	365	1082	373	462	261	548
PInc	370	546	1624	1811	429	422	423	663

Table 13 – Longterm Average End of Month Salinity Increase (EC)

	ECWeth	ECPam	ECMen	ECCawn	ECw32	ECLowDarl	ECAnnab	ECusTandou
M0	5	244	302	633	-17	-37	-41	-81
M1	4	155	366	428	-15	-29	-24	-53
M2	8	513	-217	434	-25	-67	-85	-155
M3	4	238	18	860	-13	-28	-31	-68
NoMC	9	735	-1280	-1604	-11	0	-325	-394
NoCExMO	0	-168	221	-1604	39	44	-343	-367
NoCEnMO	4	-212	288	-1604	3	14	-343	-386
0.5M	-6	-43	131	-652	-12	-9	-27	-44
NoMExCO	-1	99	-845	-736	-39	-48	6	-60
NoMEnCO	5	-178	-915	-522	-56	44	-116	-54
PInc	-6	-70	344	207	0	4	45	60

³ It should be noted that the EC changes presented in the summary tables of Appendix 3 for various locations in the Lower Murray Darling system represent the total salt load divided by the total flow volume over the full simulation period and NOT changes in end of month salinities.

Table 14 – Longterm Median End of Month Salinity (EC)

	ECWeth	EC Pam	EC Men	EC Cawn	EC w32	EC Low Darl	EC Annab	EC Cus Tandou
Base Case	354	365	415	640	386	387	334	570
M0	356	380	363	551	379	369	0	451
M1	354	381	377	564	380	373	0	472
M2	356	376	341	488	377	356	0	398
M3	352	374	392	589	381	373	0	481
NoMC	361	1349	0	0	359	359	0	240
NoCExMO	355	376	483	0	421	420	0	277
NoCEnMO	356	369	436	0	405	405	0	281
0.5M	347	363	394	605	378	379	194	556
NoMExCO	348	397	383	657	352	346	0	583
NoMEnCO	356	395	357	528	354	402	0	507
Plnc	350	370	443	688	392	393	0	615

Table 15 – Longterm Median End of Month Salinity Increase (EC)

	ECWeth	EC Pam	EC Men	EC Cawn	EC w32	EC Low Darl	EC Annab	EC Cus Tandou
M0	2	15	-52	-88	-7	-17	-334	-119
M1	0	16	-39	-76	-7	-14	-334	-99
M2	2	11	-75	-151	-10	-31	-334	-172
M3	-1	9	-24	-51	-5	-13	-334	-89
NoMC	8	984	-415	-640	-28	-28	-334	-330
NoCExMO	1	11	68	-640	34	33	-334	-293
NoCEnMO	2	4	21	-640	19	19	-334	-289
0.5M	-7	-2	-21	-35	-8	-7	-140	-14
NoMExCO	-6	32	-33	17	-34	-40	-334	13
NoMEnCO	2	30	-58	-112	-33	15	-334	-64
Plnc	-4	5	27	49	5	6	-334	45

Modelled options produce changes in salinity concentrations both within and downstream of the lakes scheme. This is discussed in the following sections.

Changes in Lake Salinity

Restoration of Lakes Menindee and Cawndilla to more natural wetting and drying cycles result in increased average salinity levels in the remaining lakes. This is due to these remaining lakes being less frequently utilised as a result of increased unregulated flows meeting demands, and the South Australian dilution flow trigger of 1,300GL being triggered less often. Consequently, there are greater periods of time when demands are low and the opportunity for concentration of salts through evaporation within the lakes is more frequent.

Restoration of Lake Menindee to natural wetting and drying appears to result in an improvement in average salinity in Lakes Cawndilla and Wetherell. However, inspection of the exceedence curves for this option reveals that results are biased by a number of extremely large monthly salinity concentrations. Median salinity levels for Lake Cawndilla and Lake Pamamaroo increase and median salinity levels for Lake Wetherell are largely unchanged.

Enhancement of the Lake Menindee restoration option through an increase in the Cawndilla outlet capacity results in improved average salinity levels in Lake Pamamaroo but a worsening of median salinity levels. Lake Pamamaroo volumes remain higher for longer periods of time as a result of Lower Darling and Murray demand now being able to be met to a greater degree from outflows from Lake Cawndilla. Whilst this results in a salinity increase for large Lake Pamamaroo volumes through lower lake utilisation, this is more than offset by the large decrease in time that the lake spends at lower levels where salinity concentrations are higher.

Restoration of Lake Cawndilla to a more natural wetting and drying cycle results in a reduction in average salinity in Lake Pamamaroo, but an increase in median salinity. There is also an increase in average and median salinity in Lake Menindee and negligible change in Lake Wetherell. Median salinity levels in Lakes Menindee and Pamamaroo increase as both storages have greater periods of time when demands are low and the opportunity for concentration of salts through evaporation are more frequent. Increasing the Menindee outlet capacity for this option results in an increased rate of draw down of Lake Menindee which in turn increases the time that the storage spends with low volumes and high salt concentrations. This in turn results in an average salinity increase from both the base case and the existing Menindee outlet configuration option.

Enhancement of the Lake Cawndilla restoration option through an increase in the Lake Menindee outlet regulator capacity results in an improvement in average salinity levels in Lake Pamamaroo. The release of water at a greater rate through the enlarged Menindee outlet reduces the demand on Lake Pamamaroo. Whilst this results in a salinity increase at higher lake volumes through lower lake utilisation, this is more than offset by the large decrease in time that the lake spends at lower levels where salinity concentrations are higher.

Rapid emptying of the lakes when in New South Wales control appears to result in increased lake average salinity levels for all but one option. Median salinity levels are largely unchanged for Lakes Wetherell and Pamamaroo, and decrease for Lakes Cawndilla and Menindee. Rapid emptying options seek to achieve savings through reductions in surface area. However, a consequence of rapid emptying is that the lakes spend a greater proportion of time at low levels where evaporative losses can lead to much higher salt concentrations.

Changes in Downstream Salinity

Downstream of the scheme, average and median salinity levels generally decrease in both the Lower Darling and in the Murray for the rapid emptying options. This is due to reduced lake evaporation losses leading to greater volumes available for dilution.

Restoration options, that involve Lake Cawndilla increase salinity concentrations in the Lower Darling and Murray. Prior to restoration these increased salt loads would have been discharged from Lake Cawndilla into the Darling Anabranch.

Restoration of Lake Menindee to more natural wetting and drying reduces salinity levels in the Lower Darling due to increased volumes of water available for dilution. However, enhancement of this option through enlargement of the Cawndilla outlet regulator to the Lower Darling results in increased salinity levels as a consequence of

this water now entering the Lower Darling in preference to the Darling Anabranch. Of interest is the apparent salinity increase in the Murray. Reasons for this are thought to be due to the substantial alteration in the South Australian dilution flow pattern.

Restoration of both Lake Menindee and Lake Cawndilla combines the effects of increased salt loads into the Lower Darling as a result of less frequent use of Lake Cawndilla, and increased dilution flows from less frequent use of Lake Menindee. The result is a reduction in salinity in both the Lower Darling and the Murray.

4.4 Variation in Dilution Flow Release Patterns

Dilution flows from the Menindee Scheme are dependent on volumes in Menindee, Hume and Dartmouth storages. The minimum trigger volume in Menindee Lakes is 1,300 Gigalitres. Inspection of the combined storage surface area versus volume relationship for the lake scheme (see Figure 14) indicates that the change in surface area for volumes in this range is small. Consequently alteration of the dilution flow pattern from 58 Gigalitres per month to a pattern in which a greater volume is realised over a smaller window is unlikely to appreciably reduce the evaporative area of water remaining in the scheme. Therefore no significant savings from this type of approach are likely to be realised. Consequently no further assessment of this option was conducted.

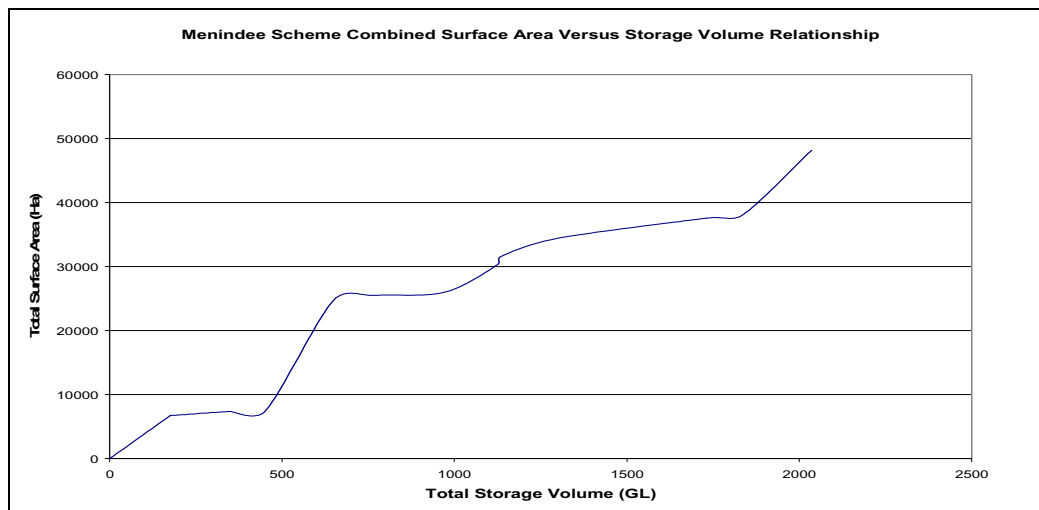


Figure 14 – Menindee Scheme Surface Area versus Volume Relationship

4.5 Potential Water Savings from Privately Owned Storages

Results from the case study analysis of options for reducing evaporative losses from off river storages are presented in Table 16. Findings are discussed in the following sections.

Table 16 - Water Savings from Privately Owned Storages (Namoi Case Study)

	Base Case	Purchase All Supplementary Water Licenses (Option 1)	No OFS, 1,000,GL in each dam (Option 2)	No Evap on OFS (Option 3)
General security (GL/Yr)	199	215	204	188
Supplementary (GL/Yr)	36	0	0	33
Floodplain harvesting (GL/Yr)	14	19	0	11
Rainfall runoff harvesting (GL/Yr)	77	77	7	71
Groundwater (GL/Yr)	34	35	36	29
End of System Flow (GL/Yr)	704	717	730	716
Average Area planted (Ha)	44,970	45,150	47,000	47,143
Sustainable area (Ha)	42,038	41,601	39,171	44,588
Keepit + Split Rock evaporation	49	47	73	47
OFS evaporation	79	77	0	0

4.5.1 Purchase of All Supplementary Licenses

As can be seen from Table 15, reduced access to supplementary water is offset by increased general security and floodplain harvesting. This is as a consequence of no corresponding lowering of the plan limit for the valley in the model. As a result evaporation in off-river storages is hardly reduced at all. Reduced access to supplementary water does however increase the Namoi end of system flows by 13 Gigalitres per annum.

If reduced access to supplementary water is accompanied by a reduction in the valley plan limit, a greater increase flow would be observed in the river and users would be forced to improve their efficiency in order to ensure maintenance of existing production levels. This would in all likelihood be through a reduction in farm storage evaporation.

4.5.2 Removal of Off-River Storage

Removal of off river storage capacity and a corresponding increase in the capacity of Keepit and Split Rock Dams results in increased evaporative losses from Keepit and Split Rock. However, this is more than offset by the reduction in evaporation from off-river storages. The total saving in evaporation from this option is 55 Gigalitres per annum. The major impact from this saving strategy is the large decrease in valley diversions. Therefore enlargement of Keepit and Split Rock cannot offset the impacts of removal of off-river storage.

4.5.3 Stopping Evaporation from Off-River Storages

Under this option evaporation from off river storages was assumed to be able to be reduced to zero. Rainfall directly into off-river storages was assumed to still be possible.

The extra water in the off river storages as a result of reduced evaporation allows users to divert less water and plant a greater area. An additional benefit is that the average volume in Keepit and Split Rock Dam also increases with little change in major storage evaporation.

5 DISCUSSION OF NON MODELLED RESULTS

5.1 Use or Creation of Upstream Storage Capacity

5.1.1 Instream Storage in The Upper Darling and Floodplain Storage at Menindee

Instream Storage in the Upper Darling

Storing water in an instream storage with a small surface area immediately upstream of the Menindee Scheme will result in reduced evaporative losses when compared to the equivalent volume being stored at the Menindee Lakes Scheme. Furthermore, the additional delivery losses are likely to be small and the ability to relocate water from the inefficient lakes scheme into the instream storage is likely to be easier if the location of the storage is in the vicinity of Menindee.

When volumes exceed the capacity of this instream storage, an operational decision will need to be made with respect to whether the instream storage is emptied and all water is stored in the lakes scheme, or alternatively whether only the volume in excess of the instream storage capacity is stored in the lake scheme. If the latter occurs then the usefulness of the additional in stream storage capacity is diminished by the increase in total surface area.

This is best shown by Figure 15 which compares the combined storage volume surface area relationships for two cases. Case 1 represents the present arrangement where water is set aside in dry times to meet Broken Hill town water supply and High Security and Riparian requirement and a drawdown sequence occurs using water in Lake Pamamaroo and then Lake Wetherell. Case 2 represents storing this same water in an instream storage in the vicinity of the scheme (at Bourke), Lake Wetherell and Lake Pamamaroo. The draw down sequence for this case would be Lake Pamamaroo first, then relocation of the water into the instream storage, then drawing down the instream storage, and then Lake Wetherell. The instream storage has a capacity of 46 GL as presented in Table 5 in the previous chapter.

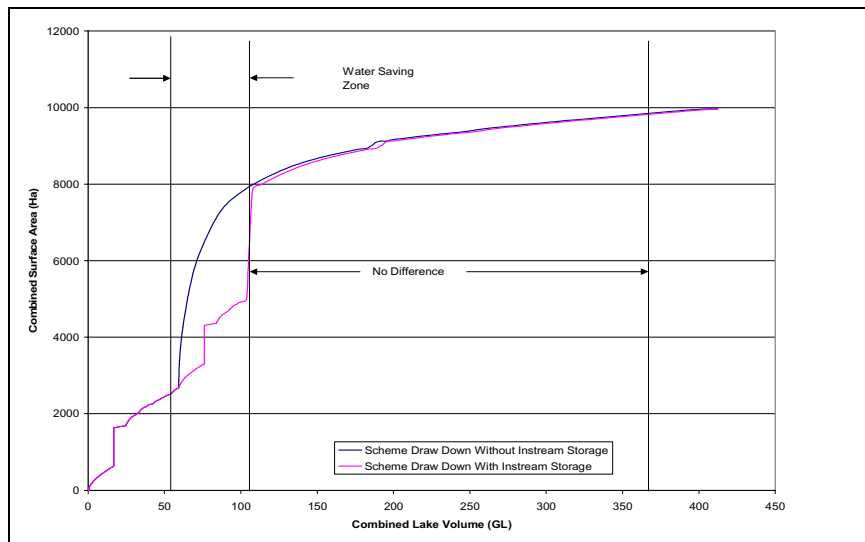


Figure 15 – Combined Storage Area versus Volume Relationship

As can be seen from Figure 15, savings through reductions in evaporation using the instream storage in Case 2 are only realised in the range of approximately 60 to 110 Gigalitres. In this zone the combined Case 2 storage surface area is less than that of Case 1 and water is not required to be stored in Lake Pamamaroo. For volumes in excess of 110 Gigalitres water is required to be held in Lake Pamamaroo resulting in surface areas equivalent to that of Case 1. Given that stored volumes are frequently in excess of 110 Gigalitres this translates to only a small long-term saving.

In conclusion, the small volume of instream storage offered upstream of the scheme together with the small volumetric range in which savings are apparent, mean that it is likely to be less attractive than some other drought security options. One such option is the creation of complimentary floodplain storage at Menindee.

Floodplain Storage at Menindee

Use of a floodplain storage in the form of a ring tank together with the previous instream storage allows water savings to be realised over a larger range of stored volumes, and reduces the need to hold drought reserves in the shallow lakes. This is particularly the case when ring tanks depths approach 6 metres.

The storage area relationship for scheme drawdown utilising water stored in an upstream instream storage, a floodplain ring tank at Menindee, and Lake Wetherell is displayed in Figure 16. The storage area relationship for scheme drawdown storing this same volume using only Lake Pamamaroo and Lake Wetherell is also shown. The ring tank is 6 m deep with a volume of 150 Gigalitres as presented in Table 6.

As can be seen the range of storage volumes over which water savings can be made is considerably larger than that of Figure 15 when only upstream instream storage is utilised.

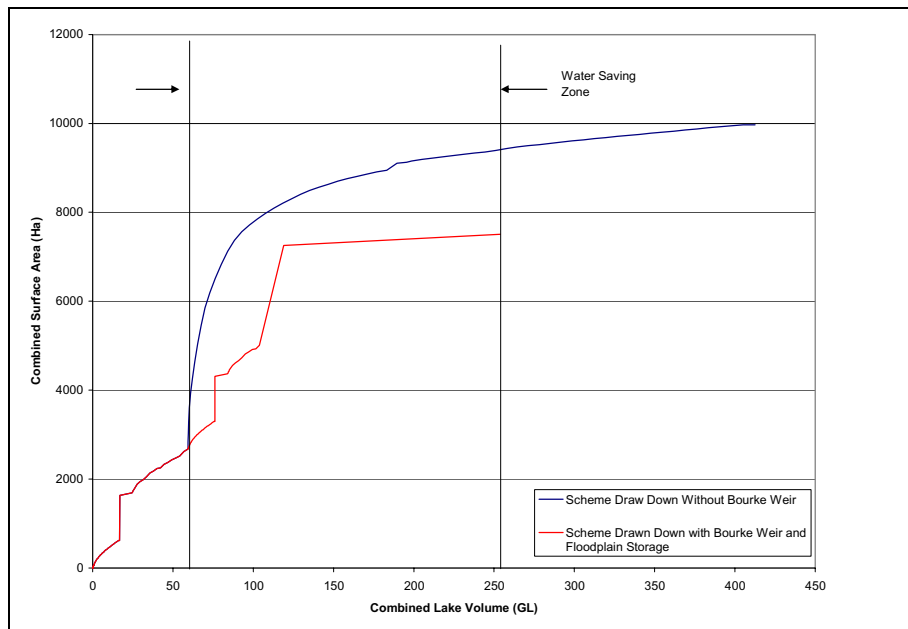


Figure 16 – Combined Storage Area Versus Volume Relationship

If the combination of Lake Wetherell and instream and floodplain storage shown in Figure 16 were used in preference to the Lake Wetherell and Lake Pamamaroo combination, 225 Gigalitres as opposed to 275 Gigalitres (refer to Figure 1) is required to meet Broken Hill, and High Security and Riparian requirements over 18 months. This is an evaporative saving of 55 Gigalitres. The distribution of resources required to achieve this is shown in Figure 17.

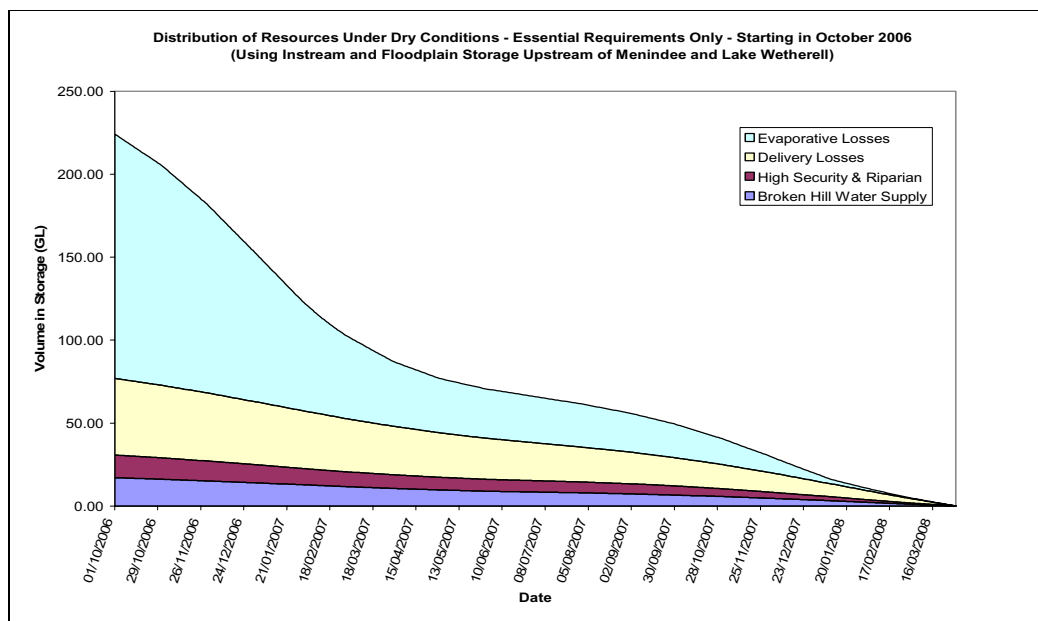


Figure 17 – Distribution of Resources Under Dry Conditions

Although this evaporative saving of 55 Gigalitres appears large it must be remembered that scheme storage is seldom in this range and that in terms of a long-term average this saving volume is considerably lesser and in the order of only 6 Gigalitres per annum.

5.1.2 Improved Use of Existing Smaller Deeper Lakes

The analysis of the proceeding section has demonstrated that creation of additional stored volumes through instream and floodplain storage have to approach 165 Gigalitres for a surface area of 5,000Ha before any appreciable evaporative savings can be made. An assessment of the saving associated with better use of existing smaller deeper lakes for drought supplies has been made. Lake Tandure has been assumed to be able to be utilised as drought security storage. Full supply capacity has been increased from the present 89 Gigalitres (RL 62.3 metres) to 129 Gigalitres (RL 64.3 metres). This assumes the construction of associated levee works and a drawdown sequence of Lake Pamamaroo, then Lake Tandure, then Lake Wetherell.

If a combination of Lake Wetherell, Lake Tandure and Lake Pamamaroo storage were used in preference to the current Lake Wetherell and Lake Pamamaroo combination, 191 Gigalitres as opposed to 275 Gigalitres (refer to Figure 1) is required to meet Broken Hill, and High Security and Riparian requirements over 18 months. This is an evaporative saving of 84 Gigalitres. The distribution of resources required to achieve this is shown in Figure 18.

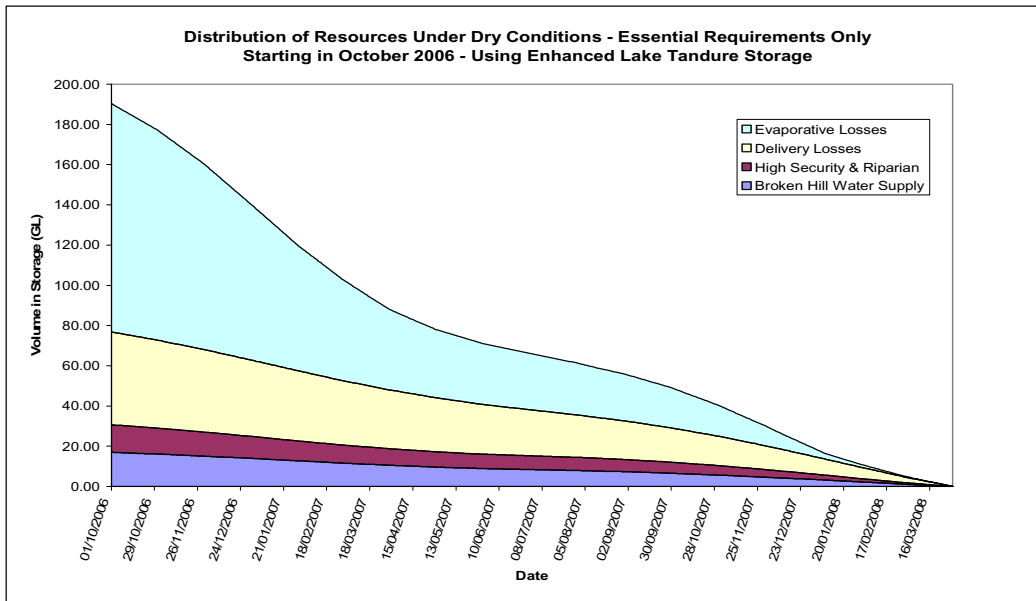


Figure 18 – Distribution of Resources Under Dry Conditions

As with the previous additional storage assessment in section 5.1.1 this evaporative saving of 84 Gigalitres is seldom realised due to the scheme seldom being in this storage range. Consequently, in terms of a long-term average this saving volume is considerably lesser and in the order of only 9 Gigalitres per annum.

5.1.3 Tributary Storages

In order to gain an appreciation of the suitability of using tributary storage in preference to Menindee scheme storage, an analysis of the losses associated with flow events along the Namoi and Barwon Darling river systems was undertaken. Small events in which there are no irrigation extractions and ungauged tributary inflows are difficult to find. Consequently, only two events for the Namoi River and one event for the Barwon-Darling were analysed.⁴

Irrigation extractions during the time of each event were not present meaning and losses are mostly attributed to the filling of in river weir storages, seepage into the bed and banks of the river and evaporation from the river surface. The progression of these events down each system is shown in Figures 19 and 20.

⁴ Note: At the time of writing this report a sustained release from Pindari Dam is being made in order to deliver water to meet downstream town water supply requirements along the Barwon Darling River. The losses associated with this event should be determined, and used as further input into the determination of delivery losses in dry times.

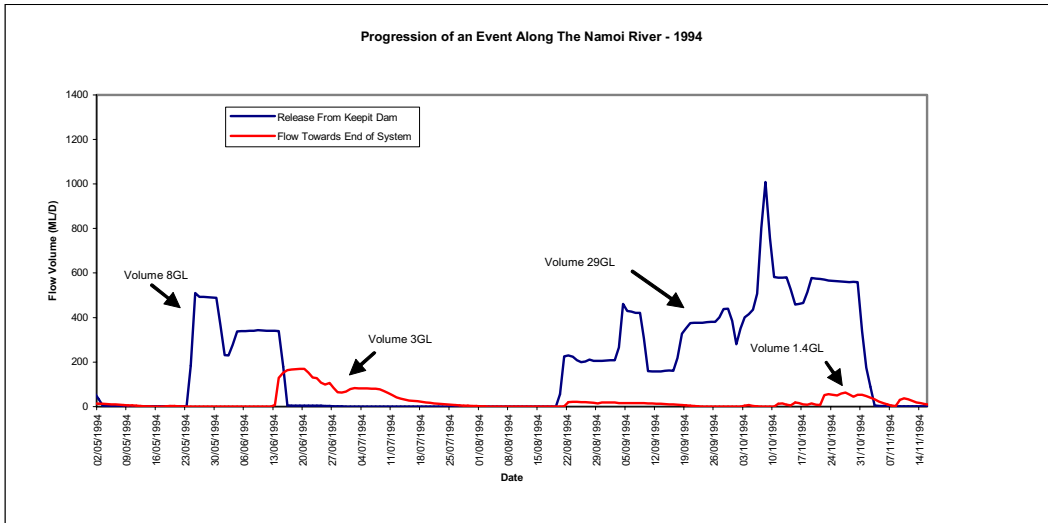


Figure 19 – Progression of Event Along the Namoi River

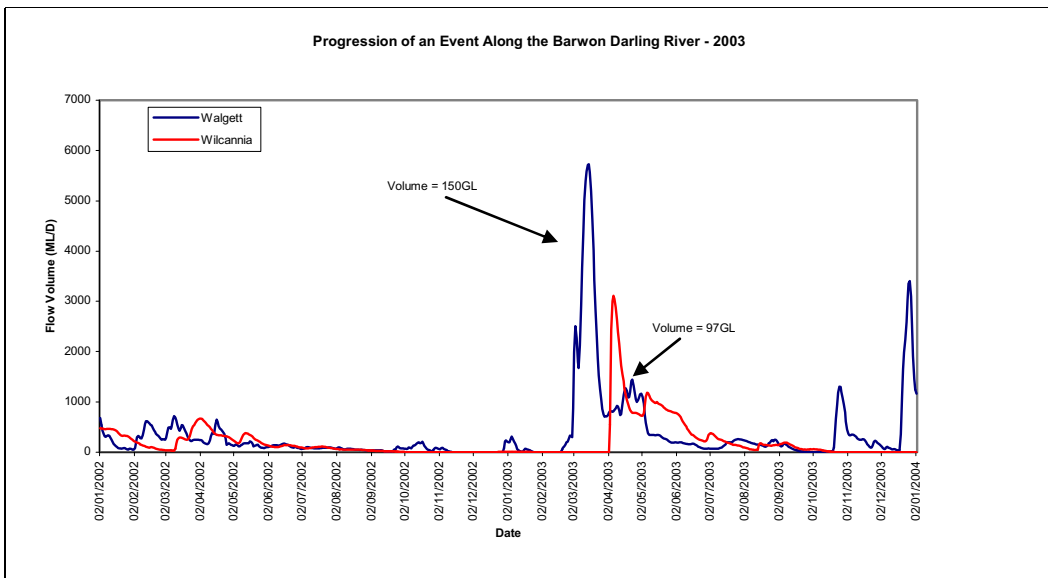


Figure 20 – Progression of Event Along the Barwon Darling River

It can be seen from the figures that large losses are experienced along both the Namoi and Barwon Darling River systems. Losses in volume for the two Namoi events in Figure 19 are 62% for the winter event and in excess of 90% for the spring event. Both of these events occurred after a period of prolonged low flows. Losses for the Barwon Darling section of the river are in the order of 35% with an initial loss of approximately 30 Gigalitres (20%) attributable to filling of the many weirs along the Barwon Darling River and the remaining 15% associated with seepage and evapo-transpiration.⁵

⁵ Losses in the Barwon Darling have only been calculated to Wilcannia, as this is the last reliable gauging point. Additional losses are likely to be incurred between Wilcannia and Menindee.

In many years the river conditions for these historic events are likely to be similar to those that would occur at times when water from the upstream storages is required for Lower Darling Water Users. Although the recent advent of environmental flows and increased end of system targets mean that losses may be slightly reduced in the case of the Namoi River from those observed in Figure 19. In addition, there may also be some years where losses can be reduced by “piggy backing” releases for scheme supply on dam environmental releases or unregulated flushes that have filled up the many weir pools along the Darling River. However, this will only be of use in years where these flushes would not have reached the Menindee Scheme.

Additional, evaporation losses attributable to storage of water in the upstream major dams is likely to be negligible due to small increases in existing dam surface areas and the required volume only being utilised at times of during times of dry conditions and low resources in Menindee Scheme.

A preliminary assessment of delivery losses associated with differing storage and delivery volumes for Keepit Dam for the Lower Darling in critical supply years was undertaken using the information from these observed events as a guide. Losses of 50% in the Namoi and an initial loss of 30 Gegalitres (for Weir filling) and a continuing loss of 15% were assumed in the Barwon Darling. In addition, information provided by State Water operational staff was also considered. Results of this assessment are presented in Table 17.

Table 17 – Possible Delivery Loss Scenarios

Keepit Released Volume (GL)	Indicative Menindee Delivered Volume (GL)	Comment
100	17	
250	80	Delivered volume equivalent to 18 Month Volume for Broken Hill, HS & Riparian, Lower Darling Delivery Losses
400	150	Delivered volume equivalent to 18 month volume for Broken Hill, HS & Riparian, Lower Darling Delivery Losses plus irrigation and water quality.

Inspection of Table 17 together with Figures 1 and 2 indicate that losses associated with either delivery of water from Keepit Dam and evaporation from Menindee Lakes is of a similar order of magnitude. The analysis also does not include any additional losses that will be incurred through temporary storage of delivered volumes within Lake Wetherell and has not assigned an environmental benefit to the losses associated with delivering water from upstream.

5.2 Use or Creation of Downstream Storage Capacity

5.2.1 Instream Storage in the Lower Darling

The small volume of instream storage in the Lower Darling (refer to Table 7) means that its usefulness in terms of storage and reduction in evaporative losses is severely limited. Consequently no further assessment of this option has taken place.

5.2.2 Instream Storage in the Murray

Additional Lock storage in the Lower Murray is not sufficient by itself to achieve significant savings. However, it could provide benefits in a refined operation strategy that allows Menindee to be emptied more rapidly and Murray Lock storage to be used as a mitigation measure. However, such a strategy would need to ensure that increased salinity and environmental impacts from increased Lock storage levels and volumes did not occur.

6 CONCLUDING REMARKS

This report has presented the results of preliminary hydrologic analysis of key water saving options within the Darling Basin. More detailed hydrologic assessment of options that appear to have merit will be required in order to fully appreciate the range of hydrologic, socio-economic and environmental implications.

Hydrologic analysis of key options has indicated that that significant water savings have been found to be possible both at the Menindee Scheme and elsewhere in the Darling Basin. However the consequences of this with respect to alterations in diversion volumes, increased salt concentrations and flow changes appears to be high.